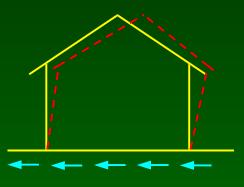


# **Background**

- Resulting force on the building can be simplified to be a lateral force - a shearing force on the base of the structure
- Force depends on:
  - earthquake intensity
  - soil conditions
  - stiffness of building





# **Determining Seismic Forces**

- ASCE 7 serves as the basis for calculating seismic forces
- · We'll use the Standard Building Code
  - methods in SBC limited to buildings < 35 ft high
- Methods determine:
  - seismic forces on members and connections
  - story drift

## **Seismic Design**

- · Complete design checks:
  - · vertical distribution of shear forces
  - · horizontal distribution of shear forces
  - overturning moment
  - story drift

• Equivalent Base Shear calculated by (1999 Standard Building Code):

$$V = C_s W$$

- V = equivalent shear force acting on the base of the structure (lbs)
- C<sub>s</sub> = seismic design coefficient
- W = total dead load of the building (lbs)

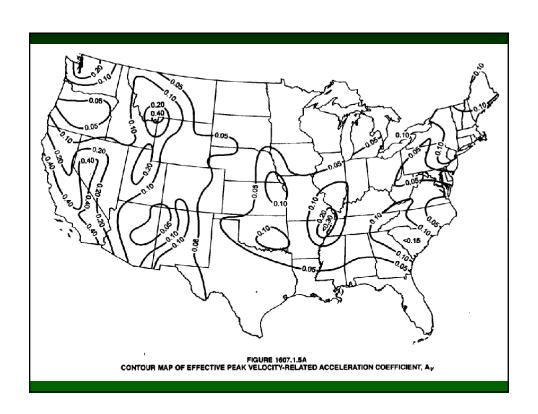
Seismic Design Coefficient C<sub>s</sub>:

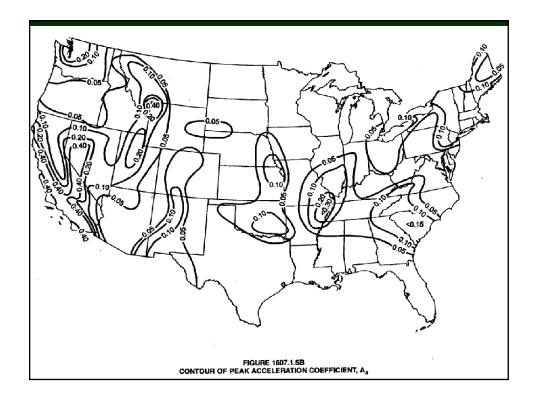
$$C_{s} = \frac{1.2 A_{v} S}{R T^{\frac{2}{3}}}$$

- A<sub>V</sub> = coefficient for peak velocity related acceleration
- S = coefficient for soil profile characteristics of the site
- R = response modification factor
- T = fundamental period of the building

- Design Step 1:
- Document the required design data:
  - Building location
  - Use of building exposure
  - Site conditions
  - Type of structure
  - Type of analysis method used

- Design Step 2:
- Find Av and Aa
  - See Figure 1607.1.5A
  - See Figure 1607.1.5B





- Design Step 3:
- Find the Seismic Hazard Exposure Group
  - See Table 1607.1.6 for the classification of the building

SEISMIC H	TABLE 1607.1.6 AZARD EXPOSURE GROUP
GROUP TYPE	NATURE OF OCCUPANCY
Group 1	All buildings except those listed below
Group II Seismic Hazard Exposure Group II buildings are those which have a substantial public hazard due to occupancy or use, including buildings containing any one or more of the indicated uses.	1. Group A in which more than 300 people congregate in one room. 2. Group E with an occupant load greater than 250. 3. Group B used for college or adult education with an occupant load greater than 500. 4. Group I Unrestrained with an occupant load greater than 50, not having surgery or emergency treatment facilities. 5. Group I Restrained. 6. Power generating stations and other public utility facilities not included in Group III Seismic Hazard Exposure Group. 7. Any other occupancy with an occupant load greater than 5,000.
Group III Seismic Hazard Exposure Group III buildings are those having essential facilities which are required for postearthquake recovery, including buildings containing any one or more of the indicated uses.	1. Fire or rescue and police stations. 2. Group I Unrestrained having surgery or emergency treatment facilities. 3. Earthquake emergency preparedness centers. 4. Postcarthquake recovery vehicle garages. 5. Power generating stations and other utilities required as emergency backup facilities. 6. Primary communication facilities. 7. Highly toxic materials as defined by 308.2.1 as an H4 occupancy where the quantity of the material exceeds the exempt amounts of Table 308.2.D.

- Design Step 4:
- Find the Seismic Performance Category
  - See Table 1607.1.8 for the performance category

TABLE 1607.1.8 SEISMIC PERFORMANCE CATEGORIES					
SEISMIC H	AZARD EXPO	SURE GROUP			
ı	II	III			
Α	Α	Α			
В	В	C			
C	C	C			
C	D	D			
D	D	Е			
	SEISMIC H	SEISMIC HAZARD EXPO			

- Design Step 5:
- Find the Site Coefficient
  - See Table 1607.3.1 for the site coefficient
  - Use 2.0 if you don't have information
  - Make sure you do the site investigation to know the soil characteristics

	TABLE 1607.3.1 SITE COEFFICIENT	
SOIL PROFILE TYPE	DESCRIPTION	SITE COEFFICIENT S
S <sub>1</sub>	A soil profile with either: Rock of any characteristic, either shale-like or crystalline in nature, which has a shear wave velocity greater than 2,500 feet per second or Stiff soil conditions where the soil depth is less than 200 feet and the soil types overlaying rock are stable deposits of sands gravels or stiff clays.	1.0
$S_2$	A soil profile with deep cohesionless or stiff clay conditions, where the soil depth exceeds 200 feet and soil types overlaying rock are stable deposits of sands, gravels, or stiff clays.	1.2
$S_3$	A soil profile containing 20 to 40 ft in thickness of soft to medium-stiff clays with or without intervening layers of cohesionless soils.	1.5
S <sub>4</sub>	A soil profile characterized by a shear wave velocity of less than 500 feet per second containing more than 40 ft of soft clay.	2.0

- Design Step 6:
- Find the Response Modification Factor, R
  - See Table 1607.3.3
- Find the Deflection Amplification Factor,  $\mathbf{C}_{\mathbf{d}}$ 
  - See Table 1607.3.3

BASIC STRUCTURAL SYSTEM						
	RESPONSE MODIFICATION	DEFLECTION		AND BUILDING H	STEM LIMITAT EIGHT (M) LIM	
Selsmic resisting system	FACTOR R	AMPLIFICATION FACTOR		Seismic Performa	nce Category	
		C.	A&B	c	D4	Es
REARING WALL SYSTEM						
Light framed walls without panels	61/2	4	NL.	NL	160	100
Reinforced concrete shear walls	41/2	2	NL.	NL	160	100
Reinforced manonry shear walls	3 1/2	i	NL.	NL.	160	100
Concentrically braced frames	4	3 1/2	NL	NL.	160	100
Unreinforced masoury shear walls	1.14	1.04	NL	Note 3	NP	NP
Plain Concrete Shear Walls	1 1/2	1 1/2	NL.	Note 3	NP	NP
BUILDING FRAME SYSTEM						
licontrically broad frames.		4	NL.	NL.	160	100
moment resisting connections at	-	~	176.	146		
columns away from link beam						
Eccentrically braced frames, non-	7	4	NL:	NL	160	100
moment resisting connections at						
columns away from link beam						
Light framed walls with shear	7	4 1/4	NL	NL	160	100
panels						
Concentrically braced frames	5	4 1/2	NL.	NL.	160	100
Reinforced concrete shear walls	5 1/2	5	NL.	NL	160	100
Reinforced masonry shear walls Unreinforced masonry shear walls	4 1/2	11/2	NL NL	NL Note 3	160 NP	NP
Plain Concrete Sheer Walls	2 2	1 1/2	NL NL	Note 3	NP NP	NP NP
Fill Coturns Show Walls	•		17th	rvae a	- AF	
MOMENT RESISTING FRAME SYSTEM						
Special moment frames of steel	8	5 1/2	NL	NL	NL	NL
Special moment frames of	8	5 1/2	NL	NL.	NL.	NL
reinforced concrete						
Intermediate moment frames of seinforced concrete	5	41/2	NL	NL.	NP	NP
Ordinary moment frames of steel	4 1/2	4	NL	NL.	160	100
Ordinary moment frames of reinforced concrete	3	2 1/2	NL	NP	NP	NP
DUAL SYSTEM WITH A SPECIAL MOM	INT FRAME CAPABLE	OF RESISTING AT LEA	AST 25% OF	THE PRESCRIBED SEIS	MIC FORCES	
Eccentrically braced frames,	8	4	NL	NL	NL	NL
moment resisting connections at						
columns away from link beam					***	600
Eccentrically braced frames non- moment resisting connections at	7	4	NL.	NL	NL	NL
columns away from link beam						
Concentrically braced frames	6	5	NL.	NL.	NL.	NL
Reinforced concrete shear walls	8	61/2	NL	NL.	NL.	NI.
Reinforced masonry shear walls	61/2	51/2	NL	NL.	NL.	NI.
Wood sheathed shear walls	8	5	NL.	NL.	NL.	NL.
DUAL SYSTEM WITH AN INTERMEDIA RESISTING AT LEAST 29% OF THE PRE	COURSED SEIGNAGE	OF RUINFORCED CONC	RETE OR A	N ORDINARY MOMENT	FRAME OF STE	EL CAPABLE
Concentrically braced frames	5	41/2	NL	NI.	160	100
Reinforced concrete shear walls	6	5	NI.	NL.	160	100
Reinforced masonry shear walls	5	41/2	NL	NL	160	100
Wood sheathed shear walls	7	4 1/2	NL	NL	160	100
INVERTED PENDULUM STRUCTURES						
Special moment frames of attractural steel	2 1/2	2 1/2	NL	NL	NL	NL
structural steel Special moment frames of	2 1/2	2 1/2	NL.	NL	NL	NL
Special moment frames of minforced concrete	a tra	2.112	DI.	NL.	PML:	NL
Dedinary moment frames of	114	1 1/4	NL.	NL.	NP	NP
structural steel						
For SIL: 1 ft = 0.305 m.		NL = not limited				
		NP = not permitte	d			
Notes						
Response modification Factor R f	e use in 1607.4 and 1	607.5. Deflection	diffication fo	ctor C. for use in 1407	4 and 1607.5	
The building height is not to exce	of the general height	imitation of Table 500	hased on th	e type of construction.		

TABLE 1607.3.31 STRUCTURAL SYSTEMS							
BASIC STRUCTURAL SYSTEM	RESPONSE	3THOCTONAL 3TO		STRUCTURAL SYS			
Seismic resisting system	MODIFICATION FACTOR R	DEFLECTION - AMPLIFICATION FACTOR		Seismic Performance Category			
		Cd	A & B	С	D4	E5	
BEARING WALL SYSTEM							
Light framed walls w/shear panels	6 1/2	4	NL	NL	160	100	
Reinforced concrete shear walls	4 1/2	4	NL	NL	160	100	
Reinforced masonry shear walls	3 1/2	3	NL	NL	160	100	
Concentrically braced frames	4	3 1/2	NL	NL	160	100	
Unreinforced masonry shear walls	1 1/4	1 1/4	NL	Note 3	NP	NP	
Plain Concrete Shear Walls	1 1/2	1 1/2	NL	Note 3	NP	NP	
BUILDING FRAME SYSTEM							
Eccentrically braced frames, moment resisting connections at columns away from link beam	8	4	NL	NL	160	100	
Eccentrically braced frames, non- moment resisting connections at columns away from link beam	7	4	NL	NL	160	100	
Light framed walls with shear oanels	7	4 1/4	NL	NL	160	100	
Concentrically braced frames	5	4 1/2	NL.	NL.	160	100	
Reinforced concrete shear walls	5 1/2	5	NI.	NL.	160	100	
Reinforced masonry shear walls	4 1/2	4	NL.	NL.	160	100	
Unreinforced masonry shear walls	1 1/2	1 1/2	NL.	Note 3	NP	NP	
Plain Concrete Shear Walls	2	2	NL	Note 3	NP	NP	
MOMENT RESISTING FRAME SYSTEM							
Special moment frames of steel	8	5 1/2	NL	NL	NL	NL	
Special moment frames of	8	5 1/2	NL	NL	NL	NL	
reinforced concrete	-						
Intermediate moment frames of	5	4 1/2	NL.	NL.	NP	NP	
reinforced concrete	-						
Ordinary moment frames of steel	4 1/2	4	NL	NL	160	100	
Ordinary moment frames of	3	2 1/2	NL.	NP	NP	NP	
reinforced concrete	-						

## • Design Step 7:

- Calculate the Fundamental Period of the building, T
  - T is from an analysis of the structural properties of the building elements
  - to estimate T, we use:

$$T = T_a C_a$$

 Calculate the Fundamental Period of the building, T

$$T = T_a C_a$$

$$\mathbf{T} = \mathbf{T_a} \mathbf{C_a}$$
 
$$\mathbf{T_a} = \mathbf{C_T} (\mathbf{h_n})^{\frac{3}{4}}$$

- C<sub>T</sub> = 0.02 for wood framed buildings with shear walls
- h<sub>n</sub> = height of building
- C<sub>a</sub> is from Table 1607.4.1.2

TABLE 1607.4.1.2 DEFFICIENT FOR UPPER LIMIT ON CALCULATED PERIOD,			
A, COEFFICIENT REPRESENTING EFFECTIVE PEAK VELOCITY-RELATED ACCELERATION	Ca		
0.4	1.2		
0.3	1.3		
0.2	1.4		
0.15	1.5		
0.1	1.7		
0.05	1.7		

- Design Step 8:
- Calculate Seismic Design Coefficient C<sub>s</sub>:

$$C_s = \frac{1.2 A_v S}{R T^{\frac{2}{3}}}$$

• C<sub>s</sub> need not be less than:

$$C_s = \frac{2.5 A_a}{R}$$

- Design Step 9:
- Calculate Dead Load of the Building, W
  - Estimate weights of all building materials and permanent fixtures
    - HVAC, plumbing, etc.

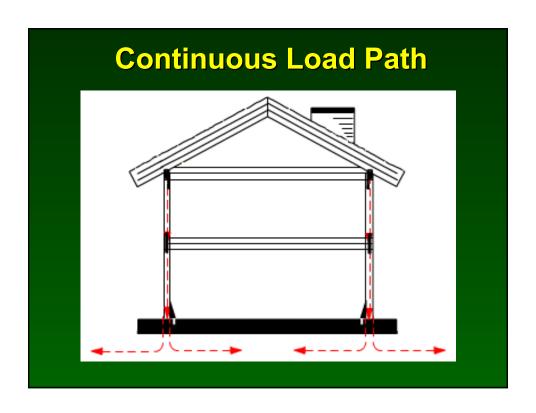
- Design Step 10:
- · Calculate base shear force:

$$V = C_s W$$

- Other Steps:
- Calculate vertical distribution of shear forces
- Calculate horizontal distribution of shear forces at each story
  - depends on relative stiffness of each vertical structural element
  - Check torsion in building

- Other Steps:
- Find overturning moments
- Calculate story drift and compare against the allowable drift
- Check building stability





# Determining Deflection Criteria

- Deflection is the main serviceability concern in structures
  - Excessive deflection in floors and roofs makes occupants feel uncomfortable
  - Excessive deflection leads to cracked ceilings, cracked walls, cracked bridge surfaces

### **Deflection Criteria**

 Deflection criteria for buildings are found in Standard Building Code (and many other design references)

CONSTRUCTION	LL	DL + LL
Roof member supporting plaster, or floor member	L/360	L/240
Roof members supporting nonplastered ceilings	L/240	L/180
Roof members not supporting ceilings	L/180	L/120
Exterior and interior walls and partitions		
with brittle finishes	L/240	_
Exterior and interior walls and partitions		
with flexible finishes	L/120	_
Farm buildings	_	L/180
Greenhouses	-	L/120

## **Deflection Criteria**

#### TABLE 1610.1 DEFLECTION LIMITS<sup>1, 2, 3, 4, 5</sup>

CONSTRUCTION	LL	DL + LL
Roof member supporting plaster, or floor member	L/360	L/240
Roof members supporting nonplastered ceilings	L/240	L/180
Roof members not supporting ceilings	L/180	L/120
Exterior and interior walls and partitions with brittle finishes	L/240	_
Exterior and interior walls and partitions		
with flexible finishes	L/120	_
Farm buildings	_	L/180
Greenhouses	-	L/120

LL = Live load

DL = Dead load

L = Length of member in same units as deflection

## **Load Combinations**

Don't forget to apply load combinations in

design

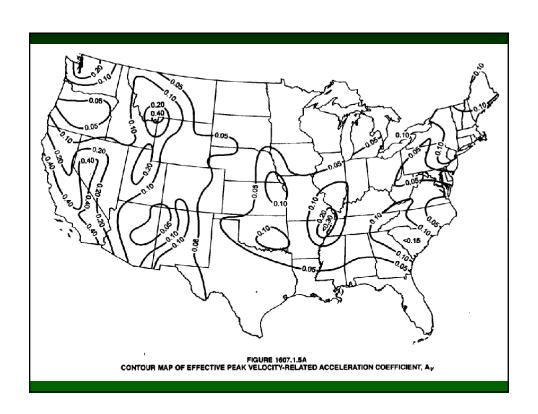
#### SECTION 1609 LOAD COMBINATIONS

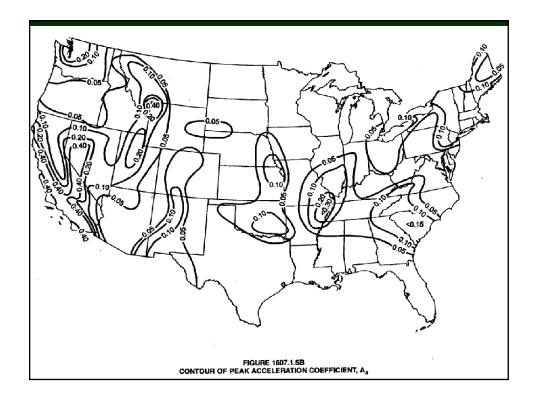
1609.1 Allowable stress design. Every building element shall be provided with sufficient strength to resist the most critical effects resulting from the following combinations of loads:

- Dead Load + Floor Live<sup>1</sup> + Roof Live (or Snow)<sup>2</sup>
- 2. Dead Load + Floor Live<sup>1</sup> + Wind (or Seismic/1.4)
- 3. Dead Load + Floor Live<sup>1</sup> + Wind + 1/2 Snow<sup>2</sup>
- 4. Dead Load + Floor Live<sup>1</sup> + 1/2 Wind + Snow<sup>2</sup>
- 5. Dead Load + Floor Live<sup>1</sup> + Snow<sup>3</sup> + Seismic/1.4

#### Notes

- Floor live load shall not be included where its inclusion results in lower stresses in the building element under investigation.
- Crane loads need not be combined with roof live load nor with more than 3/4 of snow load or 1/2 wind load.
- Snow loads over 30 psf (1.44 kPa) may be reduced no more than 80% upon approval of the building official. Snow loads 30 psf (1.44 kPa) or less need not be combined with seismic.





SEISMIC H	TABLE 1607.1.6 AZARD EXPOSURE GROUP
GROUP TYPE	NATURE OF OCCUPANCY
Group 1	All buildings except those listed below
Group II Seismic Hazard Exposure Group II buildings are those which have a substantial public hazard due to occupancy or use, including buildings containing any one or more of the indicated uses.	1. Group A in which more than 300 people congregate in one room. 2. Group E with an occupant load greater than 250. 3. Group B used for college or adult education with an occupant load greater than 500. 4. Group I Unrestrained with an occupant load greater than 50, not having surgery or emergency treatment facilities. 5. Group I Restrained. 6. Power generating stations and other public utility facilities not included in Group III Seismic Hazard Exposure Group. 7. Any other occupancy with an occupant load greater than 5,000.
Group III Seismic Hazard Exposure Group III buildings are those having essential facilities which are required for postearthquake recovery, including buildings containing any one or more of the indicated uses.	1. Fire or rescue and police stations. 2. Group I Unrestrained having surgery or emergency treatment facilities. 3. Earthquake emergency preparedness centers. 4. Postearthquake recovery vehicle garages. 5. Power generating stations and other utilities required as emergency backup facilities. 6. Primary communication facilities. 7. Highly toxic materials as defined by 308.2.1 as an H4 occupancy where the quantity of the material exceeds the exempt amounts of Table 308.2D.

## TABLE 1607.1.8 SEISMIC PERFORMANCE CATEGORIES

	SEISMIC H	AZARD EXPO	SURE GROUP	
RELATED ACCELERATION, A	ı	11	III	
$A_{\nu} < 0.05$	Α	Α	Α	
$0.05 \le A_v < 0.10$	В	В	C	
$0.10 \le A_v < 0.15$	C	C	C	
$0.15 \le A_{\nu} < 0.20$	C	D	D	
$0.20 \le A_v$	D	D	E	

TABLE 1607.3.1 SITE COEFFICIENT				
SOIL PROFILE TYPE	DESCRIPTION	SITE COEFFICIENT S		
S <sub>1</sub>	A soil profile with either: Rock of any characteristic, either shale-like or crystalline in nature, which has a shear wave velocity greater than 2,500 feet per second or Stiff soil conditions where the soil depth is less than 200 feet and the soil types overlaying rock are stable deposits of sand gravels or stiff clays.			
$S_2$	A soil profile with deep cohesionless or stiff clay conditions, where the soil depth exceeds 200 feet and soil types overlaying rock are stable deposits of sands, gravels, or stiff clays.	1.2		
$S_3$	A soil profile containing 20 to 40 ft in thickness of soft to medium-stiff clays with or without intervening layers of cohesionless soils.	1.5		
S <sub>4</sub>	A soil profile characterized by a shear wave velocity of less than 500 feet per second containing more than 40 ft of soft clay.	2.0		

TABLE 1607.3.31 STRUCTURAL SYSTEMS							
BASIC STRUCTURAL SYSTEM	RESPONSE		_	TRUCTURAL SY			
Selsmic resisting system	MODIFICATION FACTOR R	DEFLECTION - AMPLIFICATION FACTOR					
		Cª	A & B	С	D4	E5	
BEARING WALL SYSTEM							
Light framed walls w/shear panels	6 1/2	4	NL	NL	160	100	
Reinforced concrete shear walls	4 1/2	4	NL	NL	160	100	
Reinforced masonry shear walls	3 1/2	3	NL	NL	160	100	
Concentrically braced frames	4	3 1/2	NL	NL	160	100	
Unreinforced masonry shear walls	1 1/4	1 1/4	NL	Note 3	NP	NP	
Plain Concrete Shear Walls	1 1/2	1 1/2	NL	Note 3	NP	NP	
BUILDING FRAME SYSTEM							
Eccentrically braced frames, moment resisting connections at columns away from link beam	8	4	NL	NL	160	100	
Eccentrically braced frames, non- moment resisting connections at columns away from link beam	7	4	NL	NL	160	100	
Light framed walls with shear panels	7	4 1/4	NL	NL	160	100	
Concentrically braced frames	5	4 1/2	NL	NL	160	100	
Reinforced concrete shear walls	5 1/2	5	NL.	NL	160	100	
Reinforced masonry shear walls	4 1/2	4	NL	NL	160	100	
Unreinforced masonry shear walls	1 1/2	1 1/2	NL	Note 3	NP	NP	
Plain Concrete Shear Walls	2	2	NL	Note 3	NP	NP	
MOMENT RESISTING FRAME SYSTEM							
Special moment frames of steel	8	5 1/2	NL	NL	NL	NL	
Special moment frames of	8	5 1/2	NL	NL	NL	NL	
reinforced concrete							
Intermediate moment frames of reinforced concrete	5	4 1/2	NL	NL	NP	NP	
Ordinary moment frames of steel	4 1/2	4	NL	NL	160	100	
Ordinary moment frames of reinforced concrete	3	2 1/2	NL	NP	NP	NP	

# TABLE 1607.4.1.2 COEFFICIENT FOR UPPER LIMIT ON CALCULATED PERIOD, $\mathbf{C}_{\mathbf{g}}$

COEFFICIENT REPRESENTING EFFECTIVE PEAK VELOCITY-RELATED ACCELERATION	Ca
0.4	1.2
0.3	1.3
0.2	1.4
0.15	1.5
0.1	1.7
0.05	1.7