## C H A P T E R 5

## Circuit <br> Elements

| A | Heterostructure field-effect transistors (HFETs) | SPICE3 |
| :--- | :--- | :---: |
| $\mathbf{B}$ | Non-linear dependent sources | SPICE3 |
| $\mathbf{B}$ | GaAs field-effect transistor | PSPICE |
| $\mathbf{C}$ | Capacitors |  |
| $\mathbf{D}$ | Diodes |  |
| $\mathbf{E}$ | Linear voltage-controlled voltage sources |  |
| $\mathbf{F}$ | Linear current-controlled current sources |  |
| $\mathbf{G}$ | Linear voltage-controlled current sources |  |
| $\mathbf{H}$ | Linear current-controlled voltage sources |  |
| $\mathbf{I}$ | Independent current sources | SPICE3 |
| $\mathbf{J}$ | Junction field-effect transistors (JFETs) | SPICE3 |
| $\mathbf{K}$ | Coupled inductors (transformers) |  |
| $\mathbf{L}$ | Inductors |  |
| $\mathbf{M}$ | Metal oxide semiconductor field-effect transistors (MOSFETs) |  |
| $\mathbf{N}$ | Heterojunction bipolar transistors (HBTs) |  |
| $\mathbf{O}$ | Lossy transmission lines (LTRA) | SPICE3 |
| $\mathbf{Q}$ | Bipolar junction transistors (BJTs) | PSPICE |
| $\mathbf{R}$ | Resistors |  |
| $\mathbf{S}$ | Voltage-controlled switches |  |
| $\mathbf{T}$ | Lossless transmission lines |  |
| $\mathbf{U}$ | Uniform distributed $R C$ lines (URC) | SPICE3 |
| $\mathbf{U}$ | Digital devices |  |
| $\mathbf{V}$ | Independent voltage sources |  |
| $\mathbf{W}$ | Current-controlled switches |  |
| $\mathbf{X}$ | Subcircuit call |  |
| $\mathbf{Z}$ | GaAs metal semiconductor field-effect transistors (MESFETs) |  |

A circuit's topology is described by listing all circuit elements and specifying the nodes to which they are connected. Each statement describes one circuit element. Statements always start with the element name. The node numbers are then listed, and the element value or model name follows. Optional parameters may also follow the listed nodes. The name of an element always starts with a specific letter which indicates the type of element. Table 5.1 shows the list of elements and their code letters. Subsequent letters are reserved for user-defined element names. In element description and in examples SPICE keywords and letters are written using bold characters. Names that can be chosen by the user start with capital letters and italic characters are used.

For example, a capacitor name must begin with the letter $\mathbf{C}$ and can have up to eight characters (letters or digits): C2, Ccoupl, C27, and CBLOCK. The original SPICE2 version, which was written in Fortran, requires the use of capital letters. Most current SPICE programs allow both small and capital letters. In most SPICE versions, nodes numbers must be nonnegative integers but need not be numbered sequentially. In a newer SPICE programs, node can also have names described by strings of letters and digits. The number zero is always reserved for ground and must be used that way. Each node in the circuit must have a dc path to ground. Every node must have at least two connections, except for transmission line nodes (to permit unterminated transmission lines) and MOSFET substrate nodes (which actually have two internal connections ).

B - Nonlinear Dependent Source
SPICE3 only

|  | Restrictions |
| :---: | :---: |
| Bname Pnode Nnode [ $\mathbf{I}=$ Expression $][\mathbf{V}=$ Expression $]$ <br> Examples | SPICE3 |
| BN 34 I=COS(V(8)+SIN(V(13)) <br> B1 $78 \mathbf{V}=\ln \left(\boldsymbol{\operatorname { c o s }}\left(\boldsymbol{\operatorname { l o g }}\left(\mathbf{V}(3,5)^{\wedge} 2\right)\right)\right)_{-\mathbf{V}}^{(8)^{\wedge}} 3+\mathbf{V}(7)^{\wedge} \mathbf{V}(8)$ <br> B7 $1221 \mathbf{I}=1 \mathrm{~mA}$ <br> BNEW 37 V=exp(2*I(VS3)) | SPICE3 <br> SPICE3 <br> SPICE3 <br> SPICE3 |

The nonlinear source must begin with the letter B. Pnode and Nnode are the positive and negative nodes, respectively. The values of the $\mathbf{V}$ and $\mathbf{I}$ parameters determine the voltages and currents across and through the device, respectively. There is no distinction between currentcontrolled and voltage-controlled sources for the $\mathbf{B}$ element. If $\mathbf{I}=$ is given, then the device is a current source. If $\mathbf{V}=$ is given, the device is a voltage source. The small-signal ac behavior of the $\mathbf{B}$ source is a linear dependent source with a gain constant equal to the derivative (or derivatives) of the source at the dc operating point.

Expression may be any function of voltages and currents through voltage sources in the system. The source output, determined by the $\mathbf{V}=$ or $\mathbf{I}=$ option, can be either a voltage or a current. Function defined in SPICE3 program are shown in Table 5.1.

Table 5.1 Functions defined in SPICE3

| Function | Description | Units |
| :---: | :---: | :---: |
| $\mathbf{a b s}(x)$ | absolute value |  |
| $\operatorname{acos}(x)$ | arccosine | result in radians |
| $\operatorname{acosh}(x)$ | inverse hyperbolic cosine | - |
| $\operatorname{asin}(x)$ | arcsine | result in radians |
| $\operatorname{asinh}(x)$ | inverse hyperbolic sine | - |
| $\boldsymbol{\operatorname { a t a n }}(x)$ | arctan | result in radians |
| $\operatorname{atanh}(x)$ | inverse hyperbolic tangent | - |
| $\boldsymbol{\operatorname { c o s }}(x)$ | cosine | $x$ in radians |
| $\cosh (x)$ | hyperbolic cosine | - |
| $\exp (x)$ | exponential function | - |
| $\ln (x)$ | logarithm with base $e$ | - |
| $\log (x)$ | logarithm with base 10 | - |
| $\boldsymbol{\operatorname { s i n }}(x)$ | sine | $x$ in radians |
| $\sinh (x)$ | hyperbolic sine | - |
| $\operatorname{sqrt}(x)$ | square root | - |
| $\boldsymbol{\operatorname { t a n }}(x)$ | tangent | $x$ in radians |
| $\mathbf{u}(x)$ | $u(x)= \begin{cases}1 & x>0 \\ 0 & x<0\end{cases}$ | - |
| $\operatorname{uramp}(x)$ | $u(x)= \begin{cases}x & x>0 \\ 0 & x<0\end{cases}$ |  |

The following operations are defined: $+\quad$ * / ^ unary -
If the argument of $\mathbf{l o g}$, $\mathbf{l n}$, or sqrt becomes less than zero, the absolute value of the argument is used. If a divisor becomes zero or the argument of $\mathbf{l o g}$ or $\mathbf{l n}$ becomes zero, an error will result. Other problems may occur when the argument for a function in a partial derivative enters a region where that function is undefined.

To get time into an expression, you can integrate the current from a constant current source with a capacitor and use the resulting voltage to represent time. Remember to set the initial voltage across the capacitor and use UIC in the .TRAN statement.

## GASFET



| General forms | Restrictions |
| :--- | :---: |
| Bname Dnode Gnode Snode Model [Rarea] | PSPICE |
| Examples |  |
| B8 2 3 5 BMOD | PSPICE |
| B3 12 4 BMODEL 0.5 | PSPICE |

A GaAsFET is described by a statement that starts with the name of the GaAs FET device Bname. This name must start with the letter B. Node numbers Dnode, Gnode, and Snode for drain, gate, and source follows the name. Next, the model Model name is listed. Model parameters are specified in the .MODEL statement. Rarea is the relative area factor. If Rarea is not specified, 1 is assumed.

## 1. GaAs FET model

.MODEL Model_name GASFET [Model parameters]

## 2. Model parameters

In PSPICE, four different models are implemented: level 1 through level 4.

| Parameters for All Levels |  |  |  |  |
| :---: | :--- | :---: | :---: | :---: |
| Name | Parameter | Units | Default | Typical |
| LEVEL | Model index | - | 1 | 2 |
| VTO | Pinch-off voltage | V | -2.5 | -2.0 |
| BETA | Transconductance coefficient | $\mathrm{A} / \mathrm{V}^{2}$ | 0.1 | 0.1 |
| LAMBDA | Channel-length modulation parameter | $1 / \mathrm{V}$ | 0 | $10^{3}$ |


| RD | Drain ohmic resistance | $\Omega$ | 0 | 100 |
| :---: | :--- | :---: | :---: | :---: |
| $\mathbf{R S}$ | Source ohmic resistance | $\Omega$ | 0 | 100 |
| RG | Gate ohmic resistance | $\Omega$ | 0 | 10 |
| IS | Gate p-n saturation current | A | $10-^{14}$ | $10^{-14}$ |
| $\mathbf{N}$ | Gate p-n emission coefficient | - | 1 | 1.2 |
| VBI | Gate p-n potential | V | 1.0 | 0.9 |
| $\mathbf{C G S}$ | Zero-bias G-S junction capacitance | F | 0 | 5 pF |
| $\mathbf{C G D}$ | Zero-bias G-D junction capacitance | F | 0 | 5 pF |
| $\mathbf{C D S}$ | Zero-bias D-S capacitance | F | 0 | 1 pF |
| FC | Coefficient for forward-bias depletion <br> capacitance formula | - | 0.5 | 0.5 |
| EG | Bandgap voltage | eV | 1.1 | 1.4 |
| XTI | IS temperature exponent | - | 0 |  |
| VTOTC | VTO temperature coefficient | $\mathrm{V} /{ }^{\circ} \mathrm{C}$ | 0 |  |
| $\mathbf{B E T A T C E}$ | BETA exponential temperature <br> coefficient | $\% /{ }^{\circ} \mathrm{C}$ | 0 |  |
| TRG1 | RG temperature coefficient (linear) | $1 /{ }^{\circ} \mathrm{C}$ | 0 | 0.001 |
| TRD1 | RD temperature coefficient (linear) | $1 /{ }^{\circ} \mathrm{C}$ | 0 | 0.001 |
| TRS1 | RS temperature coefficient (linear) | $1 /{ }^{\circ} \mathrm{C}$ | 0 | 0.001 |
| KF | Flicker noise coefficient | - | 0 | - |
| $\mathbf{A F}$ | Flicker noise exponent | - | 1 | - |
|  |  |  |  |  |


| Parameters for Level 1 |  |  |  |  |
| :---: | :--- | :---: | :---: | :---: |
| Name | Parameter | Units | Default | Typical |
| ALPHA | Saturation voltage parameter | $1 / \mathrm{V}$ | 2.0 | 2.0 |
| TAU | Conduction current delay time | s | 0 |  |
| $\mathbf{M}$ | Gate $p n$ grading coefficient | - | 0.5 | 0.5 |


| Parameters for Level 2 |  |  |  |  |
| :---: | :--- | :---: | :---: | :---: |
| Name | Parameter | Units | Default | Typical |
| ALPHA | Saturation voltage parameter | $1 / \mathrm{V}$ | 2.0 | 2.0 |
| B | Doping tail extending parameter | $1 / \mathrm{V}$ | 0.3 | 0.3 |
| TAU | Conduction current delay time | s | 0 |  |
| $\mathbf{M}$ | Gate p-n grading coefficient | - | 0.5 | 0.5 |
| VDELTA | Capacitance transition voltage | V | 0.2 | 0.2 |
| VMAX | Capacitance limiting voltage | V | 0.5 | 0.5 |


| Parameters for Level3 |  |  |  |  |
| :---: | :--- | :---: | :---: | :---: |
| Name | Parameter | Units | Default | Typical |
| ALPHA | Saturation voltage parameter | $1 / \mathrm{V}$ | 2.0 | 2.0 |
| GAMMA | Static feedback parameter | - | 0 |  |
| DELTA | Output feedback parameter | $1 / \mathrm{AV}$ | 0 |  |
| Q | Power-law parameter | - | 2 | 2 |
| TAU | Conduction current delay time | s | 0 |  |
| $\mathbf{M}$ | Gate pn grading coefficient | - | 0.5 | 0.5 |
| VDELTA | Capacitance transition voltage | V | 0.2 | 0.2 |
| VMAX | Capacitance limiting voltage | V | 0.5 | 0.5 |


| Parameters for Level 4 |  |  |  |  |
| :---: | :--- | :---: | :---: | :---: |
| Name | Parameter | Units | Default | Typical |
| ACGAM | Capacitance modulation | - | 0 |  |
| DELTA | Output feedback parameter | $1 / \mathrm{AV}$ | 0 |  |
| Q | Power-law parameter | - | 2 | 2 |
| HFGAM | High-frequency $V_{G D}$ feedback <br> parameter | - | 0 |  |
| HFG1 | HFGAM modulation by $V_{S G}$ | $1 / \mathrm{V}$ | 0 |  |
| HFG2 | HFGAM modulation by $V_{D G}$ | $1 / \mathrm{V}$ | 0 |  |
| HFETA | High-frequency $V_{G S}$ feedback parameter | - | 0 |  |
| HFE1 | HFETA modulation by $V_{G D}$ | $1 / \mathrm{V}$ | 0 |  |


| HFE2 | HFETA modulation by $V_{G S}$ | $1 / \mathrm{V}$ | 0 |  |
| :---: | :--- | :---: | :---: | :---: |
| LFGAM | Low-frequency feedback parameter | - | 0 |  |
| LFG1 | LFGAM modulation by $V_{S G}$ | $1 / \mathrm{V}$ | 0 |  |
| LFG2 | LFGAM modulation by $V_{D G}$ | $1 / \mathrm{V}$ | 0 |  |
| MXI | Saturation knee-potential modulation | - | 0 |  |
| MVST | Subthreshold modulation | $1 / \mathrm{V}$ | 0 |  |
| P | Linear-region power law exponent | - | 2 | 2 |
| TAUD | Relaxation time for thermal reduction | s | 0 |  |
| TAUG | Relaxation time for GAM feedback | s | 0 |  |
| VBD | Gate junction breakdown potential | V | 1 | 5 |
| VST | Subthreshold potential | V | 0 | 0 |
| XC | Capacitance pinch-off reduction factor | - | 0 |  |
| XI | Saturation knee potential factor | - | 1000 |  |
| Z | Knee transition parameter | - | 0.5 |  |
| VMAX | Capacitance limiting voltage | V | 0.5 | 0.5 |

C-Capacitor

|  |  |
| :---: | :---: |
| General forms | Restriction $s$ |
| Cname Pnode Nnode Value [IC=Init_cond $]$ |  |
| Cname Pnode Nnode POLY c0 c1 c2 ... [IC=Init_cond] | SPICE2 |
| Cname Pnode Nnode [Value] [Model] [L=Length] [W=Width] [IC=Init_cond] | SPICE3 |
| Cname Pnode Nnode [Model] Value [IC=Init_cond] | PSPICE |
| Examples |  |
| CBL 30 10uF |  |
| C3 35 100nF IC=1V |  |
| CCOUP 71247 nF |  |
| C12 45 CMODEL $\mathbf{L}=10 \mathrm{u} \mathbf{W}=2 \mathrm{u}$ | SPICE3 |

This statement defines a capacitor with capacitance specified by Value (in farads) where Pnode and Nnode are the positive and negative nodes. An optional statement IC=Init_cond
specifies the initial (time-zero) voltage (in volts) on the capacitance for transient analysis. This initial condition takes effect only when the UIC option is specified in the .TRAN statement.

A nonlinear capacitor can be defined using the POLY statement where $c 0 c 1 c 2 \ldots$ are the coefficients of a polynomial describing the element value. The capacitance is expressed as a function of the voltage across the capacitor and is computed as

$$
\text { Value }=c 0+c 1 V+c 2 V^{2}+\ldots
$$

where V is the voltage across the capacitor. Although a nonlinear capacitor with keyword POLY was implemented in the original SPICE2 very few SPICE versions have this option implemented.

In SPICE3 and newer versions of SPICE the semiconductor capacitances can be declared. In this case the capacitance model is has to be specified in the .MODEL line:
.MODEL Model C [model_papramters] ...

## 1. Model parameters

| Name | Parameter | Units | Default |
| :--- | :--- | :---: | :---: |
| CJ | Junction bottom capacitance | $\mathrm{F} / \mathrm{m}^{2}$ | - |
| CJSW | Junction sidewall capacitance | $\mathrm{F} / \mathrm{m}^{2}$ | - |
| DEFW | Default device width | m | $1 \mathrm{e}-6$ |
| NARROW | Narrowing due to side etching | m | 0.0 |

This more general model for the capacitor gives you the possibility of modeling capacitance values based on geometric and process information. If Value is given then information on geometry and process will be ignored. If Model is specified, the capacitance value is calculated based on information on process and geometry using the following formula:

$$
\begin{align*}
\text { Value }= & \mathbf{C J}(\text { Length }-\mathbf{N A R R O W})(\text { Width }- \text { NARROW }) \\
& +2 \mathbf{C J S W}(\text { Length }+ \text { Width }-2 \text { NARROW }) \tag{C-1}
\end{align*}
$$

If Value is not given, then Model and Length must be specified. If Width is not given, then the model default width DEFW will be used.


| General forms | Restrictions |
| :---: | :---: |
| Dname Pnode Nnode Model [Rarea] [OFF] [IC=Vd] <br> Dname Pnode Nnode Model [Rarea] <br> Dname Pnode Nnode Modell [Rarea] [OFF] [IC=Vd] [TEMP=T] | PSPICE <br> SPICE3 |
| Examples |  |
| DREC 35 DMOD 0.2 <br> D1 712 SWITCH <br> DBRIDGE 511 DIODEM 3 <br> DCLMP 912 DMOD2 $2.0 \mathbf{I C}=0.4 \mathrm{~V}$ <br> D3 34 DMOD TEMP=25 | SPICE3 |

Dname is the device name, and for the diode it must start with the letter D. Pnode and Nnode are the anode and cathode nodes, respectively. Model is the model name, and Rarea is the relative area factor. If Rarea is not specified, 1 is assumed. An optional parameter $\mathbf{I C}=V d$ is used together with a UIC in a transient analysis. The keyword OFF indicates an optional starting condition for the dc analysis.

In SPICE3, the optional TEMP value is the temperature at which this device is to operate. It overrides the temperature specified in the .OPTION statement.

## 1. Diode model

.MODEL Model_name D [Model parameters]
2. Model parameters

| Name | Parameter | Units | Default | Typical |
| :--- | :--- | :---: | :---: | :---: |
| IS | Saturation current for Rarea $=1$ | A | $10^{-14}$ | $10^{-14}$ |
| RS | Ohmic series resistance for Rarea $=1$ | $\Omega$ | 0 | 3 |
| N | Emission coefficient | - | 1 | 1 |
| TT | Transit time | s | 0 | $10^{-9}$ |
| CJO | Zero-bias junction capacitance for Rarea $=1$ | F | 0 | $3 \cdot 10^{-12}$ |
| VJ | Junction potential | V | 1 | 0.8 |
| M | Grading coefficient | - | 0.5 | 0.5 |


| EG | Energy gap | eV | 1.11 | 1.11 |
| :--- | :--- | :---: | :---: | :---: |
| XTI | Saturation current temperature exponent | - | 3.0 | 3.0 |
| KF | Flicker noise coefficient | - | 0 | - |
| AF | Flicker noise exponent | - | 1 | - |
| FC | Coefficient for forward-bias depletion capacitance formula | - | 0.5 | - |
| BV | Reverse breakdown voltage | V | $\infty$ | 80 |
| IBV | Current at breakdown voltage | A | $10^{-3}$ | $2 \cdot 10^{-3}$ |
| TNOM | Temperature at which parameters were measured | ${ }^{\circ} \mathrm{C}$ | 27 | 27 |
|  |  |  |  |  |
|  |  |  |  |  |
| PSPICE extensions | IKF | Corner for high injection current roll-off for Rarea $=1$ | A | $\infty$ |
| TIKF | IKF temperature coefficient (linear) | $1 /{ }^{\circ} \mathrm{C}$ | 0 | 0 |
| ISR | Recombination saturation current for Rarea $=1$ | A | 0 | $10^{-8}$ |
| NR | Recombination emission coefficient | - | 2 | 2 |
| NBV | Reverse breakdown ideality factor | - | 1 | 1 |
| IBVL | Low-level reverse breakdown "knee" current for Rarea $=1$ | A | 0 | 0 |
| NBVL | Low-level reverse breakdown ideality factor | - | 1 | $10^{-8}$ |
| TBV1 | BV temperature coefficient (linear) | $1 /{ }^{\circ} \mathrm{C}$ | 0 | 0.003 |
| TBV2 | BV temperature coefficient (quadratic) | $1 /{ }^{\circ} \mathrm{C}^{2}$ | 0 | 0 |
| TRS1 | RS temperature coefficient (linear) | $1 /{ }^{\circ} \mathrm{C}$ | 0 | 0.002 |
| TRS2 | RS temperature coefficient (quadratic) | $1 /{ }^{\circ} \mathrm{C}^{2}$ | 0 | 0 |

## Examples:

*Diode small power
.MODEL 1N3879 D ( IS=1.6e-18 BV=50 IBV=10u M=0.27 CJO=100p RS=9m TT=0.3u )
*Switching diode
.MODEL 1N4148 D(IS=0.1p RS=16 CJO=2p TT=12n BV=100 IBV=0.1p)
*Rectifier diode with 400 V breakdown voltage and 25 A
.MODEL 1N3494 D (IS=5E-14 BV=400 IBV=0.001 M=0.84 CJO=1.5NF RS=3m TT=8u)
*Germanium diode
.MODEL $1 \mathrm{~N} 5817 \mathrm{D}(\mathrm{N}=1.2 \mathrm{IS}=20 \mathrm{U}$ RS=. $08 \mathrm{EG}=.69 \mathrm{XTI}=2 \mathrm{CJO}=200 \mathrm{p}$ BV=25 IBV=.01m
$+\mathrm{M}=.523 \mathrm{VJ}=2$ )

* Zener diode, 6.8 V
.MODEL $1 \mathrm{~N} 754 \mathrm{D}(\mathrm{IS}=1 \mathrm{E}-15 \mathrm{RS}=.25 \mathrm{CJO}=150 \mathrm{p} \mathrm{M}=.55 \mathrm{VJ}=.75 \mathrm{ISR}=2 \mathrm{n} \mathrm{BV}=6.8 \mathrm{IBV}=20 \mathrm{~m})$
* Variable-capacitance diode
.MODEL MV2201 D(IS=1p CJO=15p M=.4261 VJ=. $75 \quad \mathrm{FC}=.5 \quad \mathrm{BV}=25 \mathrm{IBv}=10 \mathrm{u})$

E - Voltage-Controlled Voltage Source

| Pinp ○ <br> General forms | Restrictions |
| :---: | :---: |
| Ename Pnode Nnode Pinp Ninp Gain |  |
| Ename Pnode Nnode POLY(Dimensions) Pinp Ninp ... Coef... | PSPICE |
| Ename Pnode Nnode VALUE $=\{$ Expression $\}$ | PSPICE |
| Ename Pnode Nnode TABLE $\{$ Expression $\}=($ Input, Output) ... | PSPICE |
| Ename Pnode Nnode LAPLACE $\{$ Expression $\}=\{$ Transf_expression $\}$ | PSPICE |
| Ename Pnode Nnode CHEBYSHEV $\{$ Expression $\}=\{\mathbf{L B}\|\mathbf{H P}\| \mathbf{B P} \mid \mathbf{B R}\}$ | PSPICE |
| + Freql Freq2 ... Atten1 Atten2 ... <br> Ename Pnode Nnode FREQ $\{$ Expression $\}=\left[[\mathbf{M A G} \mid \mathbf{D B}][\mathbf{D E G} \mid \mathbf{R A D}] \mid \mathbf{R} \_\mathbf{I}\right]$ + (Freq Magnitude Phase) ... [DELAY = Delay $]$ | PSPICE |
| Examples |  |
| E3 43972.0 |  |
| EBUFF 3746100 |  |
| EAMP 46 POLY(1) 58010 | PSPICE |
| ENL 1011 POLY (2) 70830.07 .50 .12 m | PSPICE |
| E13 50 VALUE $=\{12 * \operatorname{SQRT}(\mathrm{~V}(5,2))\}$ | PSPICE |
| E3 45 TABLE $\{\mathrm{V}(3)-\mathrm{V}(1)\}=(-2,4.2)(0,0)(3,5.6)(5,6)$ | PSPICE |
| E1220 TABLE $\{\mathrm{V}(3,8)\}=(0,0)(25,1)$ | PSPICE |
| E3 80 LAPLACE $\{\mathrm{V}(7)\}=\{1 /(1+0.1 * \mathrm{~s})\}$ | PSPICE |
| ELP 60 CHEBYSHEV $\{\mathrm{V}(7)\}=$ LP 1.6 k 2.5 K 0.5 dB 60 dB | PSPICE |
| ELP 70 FREQ $\{\mathrm{V}(8)\}=(0,0,0)(1 \mathrm{kHz}, 0,0)(1.5 \mathrm{kHz},-45,0)$ DELAY $=1 \mathrm{~ms}$ | PSPICE |

The first of the general forms applies for linear sources, and this form is used in SPICE2 and SPICE3. Other forms are PSPICE extensions. Pnode is the positive node, and Nnode is the negative node. Pinp and Ninp are the positive and negative controlling nodes, respectively. Gain is the voltage gain. POLY(Dimensions) specifies the number of dimensions of the polynomial. The number of pairs of controlling nodes must be equal to the number of dimensions. A particular node may appear more than once, and the output and controlling nodes need not be different. The Coef parameter specifies coefficients of the polynomial.

The VALUE, TABLE, LAPLACE, FREQ, and CHEBYSHEV forms are part of the analog behavioral modeling feature of PSPICE. The TABLE form has a maximum size of 2048 input/output value pairs. If a DELAY value is specified, the simulator will modify the phases in the FREQ table to incorporate the specified delay value. This is useful for tables which the simulator identifies as being noncausal. When this occurs, the simulator provides a delay value necessary to make the table causal. The new syntax allows this value to be specified in subsequent simulation runs, without requiring the user to modify the table.

## 1. Function used in PSPICE

The functions can be used in the PSPICE expressions are listed in Table 5.2.
Table 5.2 Functions used in PSPICE

| Function | Description | Comments |
| :---: | :---: | :---: |
| $\operatorname{ABS}(x)$ | $\|x\|$ |  |
| $\operatorname{ACOS}(x)$ | arccosine | $-1.0 \leq x \leq 1.0$ |
| ARCTAN( $x$ ) | arctangent | result in radians |
| $\operatorname{ASIN}(x)$ | arcsine | result in radians |
| ATAN $(x)$ | arctangent | result in radians |
| ATAN2 $(y, x)$ | $\tan ^{-1}(y / x)$ | result in radians |
| $\operatorname{COS}(x)$ | $\cos (x)$ | $x$ in radians |
| $\operatorname{COSH}(x)$ | hyperbolic cosine |  |
| DDT ( $x$ ) | time derivative of $x$ | only for transient analysis |
| $\boldsymbol{\operatorname { E X P }}(x)$ | $e^{x}$ |  |
| $\mathbf{I F}(t, x, y)$ | $\begin{aligned} & x \text { if } t=\text { TRUE } \\ & y \text { if } t=\text { FALSE } \end{aligned}$ | $t$ is a Boolean expression; $x$ and $y$ are either numerical values or expressions |
| IMG(x) | imaginary part of $x$ | returns 0 for real numbers |
| $\mathbf{L I M}\left(x\right.$, min, max ${ }^{\text {a }}$ | $\min$ if $x<$ min $\max$ if $x>\max$ $x$ otherwise |  |
| LOG (x) | logarithm with base $e$ |  |
| LOG10(x) | logarithm with base 10 |  |
| M $(x)$ | magnitude of $x$ | the same as $\mathbf{A B S}(x)$ |
| $\mathbf{M A X}(x, y)$ | maximum of $x$ and $y$ |  |
| $\mathbf{M I N}(x, y)$ | minimum of $x$ and $y$ |  |
| $\mathbf{P}(x)$ | phase of $x$ | returns 0 for real numbers |
| $\mathbf{P W R}(x, y)$ | $\|x\|^{y}$ | can be replaced by $\left\{x^{* *} y\right\}$ |
| $\operatorname{PWRS}(x, y)$ | $\begin{aligned} & \|x\|^{y} \text { if } x>0 \\ & -\|x\|^{y} \text { if } x<0 \\ & \hline \end{aligned}$ |  |
| $\mathbf{R}(x)$ | real part of $x$ |  |
| SGN( $x$ ) | $\begin{aligned} & \hline 1 \text { if } x>0 \\ & 0 \text { if } x=0 \\ & -1 \text { if } x<0 \end{aligned}$ | signum function |
| SIN $(x)$ | $\sin (x)$ | $x$ in radians |
| SINH $(x)$ | hyperbolic sine |  |
| SQRT $(x)$ | square root |  |
| STD $(x)$ | time integral of $x$ | only for transient analysis |
| $\operatorname{STP}(x)$ | $\begin{aligned} & \hline 1 \text { if } x>0 \\ & 0 \text { if } x \leq 0 \\ & \hline \end{aligned}$ | step function |
| TABLE $\left(x, x_{v}, x_{2}, \ldots, x_{v}, y_{n}\right)$ | piecewise characteristics |  |
| TAN $(x)$ | tangent | $x$ in radians |
| TANH ( $x$ ) | hyperbolic tangent |  |
|  |  |  |

Chebyshev filters have two attenuation values, given in dB , which specify the pass-band ripple and the stop-band attenuation. They may be given in either order. Low-pass (LP) and high pass (HP) have two cutoff frequencies, specifying the pass-band and stop-band edges, while band- pass (BP) and band-reject (BR) filters must have four.

## F - Current-Controlled Current Source



| General forms | Restrictions |
| :--- | :---: |
| Fname Pnode Nnode Vname Gain | PSPICE |
| Fname Pnode Nnode POLY(dimensions) Vname ... coef... |  |
|  |  |
| FSEN 7 8 VSENSE 180 |  |
| F5 5 9 VINP 50 |  |
| F7 4 8 VINP 100 |  |
| FA 4 7 POLY(1) VIN 0 1k | PSPICE |
| FNL 5 8 POLY(2) VCTRL1 VCTRL2 0.0 7.3 0.1 0.01 | PSPICE |

The first of the general form applies to the linear case. Vname is the name of a voltage source through which the controlling current flows. Gain is the current gain, Pnode is the positive node, and Nnode is the negative node. Current is directed from the positive node, through the source, to the negative node. The current through the controlling voltage source determines the output current. The direction of positive controlling current is from the positive node, through the source, to the negative node of Vname. The controlling source must be an independent voltage source ( $\mathbf{V}$ device).

The second form is a PSPICE extension for the nonlinear case. POLY(dimensions) specifies the number of dimensions of the polynomial. The number of controlling voltage sources must be equal to the number of dimensions.

G - Voltage-Controlled Current Source

| Pinp o <br> Ninp 。 <br> General forms | Restrictions |
| :---: | :---: |
| Gname Pnode Nnode Pinp Ninp Gm |  |
| Gname Pnode Nnode POLY(Dimensions) Pinp Ninp ... Coef ... | PSPICE |
| Gname Pnode Nnode VALUE $=\{$ Expression $\}$ | PSPICE |
| Gname Pnode Nnode TABLE $\{$ Expression $\}=($ Input, Output) ... | PSPICE |
| Gname Pnode Nnode LAPLACE $\{$ Expression $\}=\{$ Transf_expression $\}$ | PSPICE |
| Gname Pnode Nnode CHEBYSHEV $\{$ Expression $\}=\{\mathbf{L B}\|\mathbf{H P}\| \mathbf{B P} \mid \mathbf{B R}\}$ | PSPICE |
| + Freq1 Freq2 ... Atten1 Atten2 ... <br> Gname Pnode Nnode FREQ $\{$ Expression $\}=\left[[\mathbf{M A G} \mid \mathbf{D B}][\mathbf{D E G} \mid \mathbf{R A D}] \mid \mathbf{R} \_\mathbf{I}\right]$ <br> + ( Freq Magnitude Phase) ... [DELAY = Delay $]$ | PSPICE |
| Examples |  |
| G123 111310.0 |  |
| GBUFF 1210111.0 |  |
| GAMP 48 POLY(1) 370.0100 .0 | PSPICE |
| GNL 38 POLY(2) 29100.07 .70 .10 .001 | PSPICE |
| GSQRT 50 VALUE $=\{5 \mathrm{~V} * \operatorname{SQRT}(\mathrm{~V}(3,2))\}$ | PSPICE |
| GT2 30 TABLE $\{\mathrm{V}(4,8)\}=(0,0)(50,1)$ | PSPICE |
| GRC 40 LAPLACE $\{\mathrm{V}(5)\}=\{1 /(1+.01 * \mathrm{~s})\}$ | PSPICE |
| GLP 70 CHEBYSHEV $\{\mathrm{V}(4)\}=$ LP 1.6 k 2.5 k .2 dB 40 dB | PSPICE |
| GLP 60 FREQ $\{\mathrm{V}(4)\}=(0,0,0)(1 \mathrm{kHz}, 0,0)(3 \mathrm{kHz},-45,0)$ DELAY $=2 \mathrm{~ms}$ | PSPICE |
| GPSK 48 VALUE $=\{2 \mathrm{~mA} * \sin (6.28 * 10 \mathrm{kHz} *$ TIME+V(8) $)\}$ | PSPICE |
| GT 49 VALUE $=\{20 \mathrm{E}-6 * \mathbf{P W R}(\mathrm{~V}(1) * \mathrm{~V}(2), 1.5)\}$ | PSPICE |
| GLOSSY $36 \mathbf{L A P L A C E}\{\mathrm{~V}(3)\}=\left\{\exp \left(-\mathrm{sqrt}\left(\mathrm{C} * \mathrm{~s}^{*}(\mathrm{R}+\mathrm{L} * \mathrm{~s})\right)\right.\right.$ ) $\}$ | PSPICE |

The first form applies for linear sources and is used in SPICE2 and SPICE3. Other forms are PSPICE extensions. Pnode is the positive node, and Nnode is the negative node. Positive current goes from the positive node through the source to the negative node. Pinp and Ninp are the positive and negative controlling nodes, respectively. $G m$ is the transconductance in A/V. POLY(Dimensions) specifies the number of dimensions of the polynomial. The number of pairs of controlling nodes must be equal to the number of dimensions. A particular node may appear more than once, and the output and controlling nodes need not be different. The Coef parameter specifies coefficients of the polynomial. Valid expressions for PSPICE are described with E source.

The VALUE, TABLE, LAPLACE, FREQ, and CHEBYSHEV forms are part of the analog behavioral modeling feature of PSPICE. The TABLE form has a maximum size of 2048 input/output value pairs. If a DELAY value is specified, the simulator will modify the phases in the FREQ table to incorporate the specified delay value. This is useful for tables which the simulator identifies as being noncausal. When this occurs, the simulator provides a delay value
necessary to make the table causal. The new syntax allows this value to be specified in subsequent simulation runs, without requiring the user to modify the table.

Chebyshev filters have two attenuation values, given in dB , which specify the pass band ripple and the stop-band attenuation. They may be given in either order. Low-pass ( $\mathbf{L P}$ ) and high-pass (HP) have two cutoff frequencies, specifying the pass-band and stop-band edges, while band- pass ( $\mathbf{B P}$ ) and band-reject ( $\mathbf{B R}$ ) filters must have four.

## H - Current-Controlled Voltage Source



| General forms | Restrictions |
| :--- | :---: |
| Hname Pnode Nnode Vname Rm |  |
| Hname Pnode Nnode POLY(dimensions) Vname... Coef... | PSPICE |
|  |  |
| HSEN 3 7 V12 50.0 |  |
| HAMP 3 9 POLY(1) VINP 0.0 100.0 | PSPICE |
| HNL 4 8 POLY(2) VCTRL1 VCTRL2 0.0 5.8 0.1 0.02 | PSPICE |

The first general form applies to the linear source. Vname is the name of a voltage source through which the controlling current flows, $R m$ is the transresistance, Pnode is the positive node, and Nnode is the negative node of the output voltage source. The current through the controlling voltage source determines the output current. The direction of positive controlling current is from the positive node, through the source, to the negative node of Vname. The controlling source must be an independent voltage source ( $\mathbf{V}$ device).

The second form is the PSPICE extension for the nonlinear case. POLY(dimensions) specifies the number of dimensions of the polynomial. The number of controlling voltage sources must be equal to the number of dimensions.

## I-Independent Current Source



| General forms | Restrictions |
| :---: | :---: |
| Iname Pnode Nnode [[DC] Value] [[AC] Mag [Phase]] [Signal_shape] |  |
| Iname Pnode Nnode [[DC] Value] [[AC] Mag [Phase]] | PSPICE |
| + [STIMULUS = Name ] [Signal_shape] |  |
| Iname Pnode Nnode [[DC] Value] [[AC] Mag [Phase]] [Signal_shape] + [DISTOF1 F1mag [F1phase]] [DISTOF2 F2mag [F2phase]] | SPICE3 |
| Examples |  |
| ISRC 48 AC 0.33345 .0 |  |
| INP 59 DC 1V AC 1mV 90 |  |
| IPULSE 30 PULSE (0 1 mA 5 ns 1 ns 1 ns 100 ns 200 ns ) |  |
| I4 47 DC 5V AC 1 mV SIN( 0.010 .0011 MEGHz ) |  |
| I9 69 AC 0.160 SFFM (0 1 100kHz 0.51 kHz ) |  |
| IIN3 30 AC 1M DISTOF1 DISTOF2 0.001 | SPICE3 |

A current source of positive value will force current out of the Pnode node, through the source, and into the Nnode node. Value is the dc and transient analysis value of the source. If the source value is time-invariant (e.g., a power supply), then the value may optionally be preceded by the letters DC.

Mag is the ac magnitude and Phase is the ac phase. The source is set to this value in the ac analysis. If Mag is omitted following the keyword AC, a value of unity is assumed. If Phase is omitted, a value of zero is assumed. If parameters other than source values are omitted or set to zero, the default values shown will be assumed. If a source is assigned a time-dependent value, the time-zero value is used for dc analysis.

The keyword STIMULUS is used in newer versions of PSPICE to call up custom signal shapes created with the stimulus editor. By specifying Signal_shape, a time-dependent waveform for transient analysis can be assigned. If a source is assigned a time-dependent value, the time-zero value is used for dc analysis. There are five independent source functions: pulse, exponential, sinusoidal, piecewise linear, and single-frequency FM. These five signal shapes are described in more detail in what follows.

## 1. Pulse waveforms

Form
PULSE (I1 I2 TD TR TF PW PER )
Examples: I5 50 PULSE(-1mA 1mA 5ns 2ns 2ns 50 ns 100 ns )
I8 70 PULSE(0 5mA 5us 1us 1us 20us 50us)

| Parameters | Meaning | Default | Units |
| :---: | :--- | :---: | :---: |
| I1 | Initial value |  | A |
| I2 | Pulsed value |  | A |
| TD | Delay time | 0.0 | s |
| TR | Rise time | Tstep | s |
| TF | Fall time | Tstep | s |
| PW | Pulse width | Tstop | s |
| PER | Period | Tstop | s |

Parameters Tstep and Tstop are specified in the .TRAN statement.


## 2. Sine waves

Form
SIN(IO IA FREQ TD DF PHASE)
Examples: I4 40 SIN(0 1mA 10kHz 10us 1k)
I7 39 SIN(0 5mA 1kHz)

| parameters | meaning | default | units | Restrictions |
| :---: | :--- | :---: | :---: | :---: |
| IO | Offset |  | A |  |
| IA | Amplitude |  | A |  |
| FREQ | Frequency | $1 /$ Tstop | Hz |  |
| TD | Delay | 0.0 | sec |  |
| DF | Damping factor | 0.0 | $1 / \mathrm{sec}$ |  |
| PHASE | Phase | 0.0 | degre <br> e | PSPICE |



$$
\begin{equation*}
\mathbf{I}_{\mathbf{S}}=\mathbf{I} \mathbf{A} \sin \left(2 \pi \frac{\mathbf{P H A S E}}{360}\right) \tag{I-1}
\end{equation*}
$$

The shape of the waveform is described by the following expressions:
For time < TD:
$\mathbf{I O}+\mathbf{I A} \sin \left[2 \pi\left(\frac{\mathbf{P H A S E}}{360}\right)\right]$
For time > TD:
$\mathbf{I O}+\mathbf{I A} \exp [-($ time $-\mathbf{T D}) \mathbf{T H E T A}] \sin \left[2 \pi\left(\right.\right.$ FREQ $($ time $\left.\left.-\mathbf{T D})+\frac{\text { PHASE }}{360}\right)\right]$

## 3. Exponential waveforms

Format
EXP(I1 I2 TD1 TAU1 TD2 TAU2)
Examples: $\quad$ I5 $50 \mathbf{E X P}(-5 m A 1 m A 2 n s ~ 30 n s ~ 60 n s ~ 40 n s) ~$ I12 $45 \mathbf{E X P}(5 \mathrm{~mA} 5 \mathrm{us} 10 \mathrm{~ns} 15 \mathrm{~ns} 18 \mathrm{~ns})$

| Parameters | Meaning | Default | Units |
| :---: | :--- | :---: | :---: |
| I1 | Initial value |  | A |
| I2 | Pulsed value |  | A |
| TD1 | Rise delay time | 0.0 | s |
| TAU1 | Rise time constant | Tstep | s |
| TD2 | Fall delay time | TD1+Tstep | s |
| TAU2 | Fall time constant | Tstep | s |



The shape of the waveform is described by the following equations:
For time < TD1:

$$
\begin{equation*}
i(\text { time })=0 \tag{I-4}
\end{equation*}
$$

For TD1 < time < TD2:

$$
\begin{equation*}
i(\text { time })=\mathbf{I} \mathbf{1}+(\mathbf{I} \mathbf{2}-\mathbf{I} \mathbf{1})\left[1-\exp \left(-\frac{\text { time }-\mathbf{T D} \mathbf{1}}{\mathbf{T A U 1}}\right)\right] \tag{I-5}
\end{equation*}
$$

For time > TD2:
$i($ time $)=\mathbf{I} 1+(\mathbf{I} 2-\mathbf{I} 1)\left[1-\exp \left(-\frac{\text { time }-\mathbf{T D 1}}{\mathbf{T A U 1}}\right)\right]+(\mathbf{I} 1-\mathbf{I} 2)\left[1-\exp \left(-\frac{\text { time }-\mathbf{T D 2}}{\mathbf{T A U 2}}\right)\right]$

## 4. Piecewise linear waveforms

Format: $\quad$ PWL(T1 I1 [Tn In ] ... )
Example: ICLOCK 75 PWL(0-7 10NS -7 11NS -3 17NS -3 18NS -7 50NS -7)

| Parameters | Meaning | Default | Units |
| :---: | :---: | :---: | :---: |
| Tn | Time at corner | - | s |
| In | Current at corner | - | A |

Each pair of values (Tn, In) specifies the value of the source In (in A) at time=Tn. The value of the source at intermediate values of time is determined by using linear interpolation of the input values.


## 5. FM waveforms

Form

Examples:

SFFM (IO IA FC MDI FS)
I7 $60 \mathbf{S F F M}(01 \mathrm{~mA} 10 \mathrm{kHz} 0.51 \mathrm{kHz})$ I3 34 SFFM( 5 mA 1 mA 200 kHz 0.75 kHz )

| Parameters | Meaning | Default | Units |
| :---: | :--- | :---: | :---: |
| IO | Offset | - | A |
| IA | Amplitude | - | A |
| FC | Carrier frequency | $1 /$ Tstop | Hz |
| MDI | Modulation index | 0 |  |
| FS | Signal frequency | $1 /$ Tstop | Hz |



The SFFM (single-frequency frequency-modulated) waveform is described by the following equation:

$$
\begin{equation*}
i(\text { time })=\mathbf{I O}+\mathbf{I} \mathbf{A} \sin [2 \pi \mathbf{F C} \text { time }+\mathbf{M D I} \sin (2 \pi \mathbf{F S} \text { time })] \tag{I-7}
\end{equation*}
$$



| General forms | Restrictions |
| :---: | :---: |
| Jname Dnode Gnode Snode Model [Rarea] [0FF] [IC=Vds, Vgs] | SPICE2 |
| Jname Dnode Gnode Snode Model [Rarea] | PSPICE |
| Jname Dnode Gnode Snode Model $[$ Rarea $][\mathbf{O F F}][\mathbf{I C}=V d s$, Vgs] $+[$ TEMP $=T]$ | SPICE3 |
| Examples |  |
| J4 359 JMOD |  |
| J2927JM1 OFF | SPICE2/3 |

JFET is described by a statement that starts with the name of the JFET device Jname. This name must start with the letter J. Node numbers Dnode, Gnode, and Snode for drain, gate, and source follows the name. Next the model Model name is listed. Model parameters are specified in the .MODEL statement. Keywords NJF and PJW are used there for $n$-channel and $p$-channel, respectively. Rarea is the relative area factor. If Rarea is not specified, 1 is assumed. In SPICE2 and SPICE3, an optional parameter IC= $V d$ is used together with an UIC in a transient analysis. Keyword OFF indicates an optional starting condition for dc analysis. In SPICE3, different temperatures can be set for individual transistors using the keyword TEMP.

## 1. JFET models

.MODEL Model_name NJF [Model parameters]
.MODEL Model_name PJF [Model parameters]

## 2. Model parameters

| Name | Parameter | Units | Default | Typical |  |  |  |  |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| VTO | Threshold voltage | V | -2.0 | -2.0 |  |  |  |  |  |
| BETA | Transconductance parameter | $\mathrm{A} / \mathrm{V}^{2}$ | $10^{4}$ | $10^{-4}$ |  |  |  |  |  |
| LAMBDA | Channel-length modulation parameter | $1 / \mathrm{V}$ | 0 | 0 |  |  |  |  |  |
| RD | Drain resistance | $\Omega$ | 0 | 20 |  |  |  |  |  |
| RS | Source resistance | $\Omega$ | 0 | 20 |  |  |  |  |  |
| CGS | Zero-bias $G$-S junction capacitance | F | 0 | 5 pF |  |  |  |  |  |
| CGD | Zero-bias $G$-D junction capacitance | F | 0 | 5 pF |  |  |  |  |  |
| PB | Gate junction potential | V | 1 | 0.8 |  |  |  |  |  |
| IS | Gate junction saturation current | A | $1.0^{-14}$ | $1.0^{-15}$ |  |  |  |  |  |
| KF | Flicker noise coefficient | - | 0 |  |  |  |  |  |  |
| AF | Flicker noise exponent | - | 1 | 1 |  |  |  |  |  |
| FC | Coefficient for forward-bias depletion <br> capacitance formula | - | 0.5 | 0.5 |  |  |  |  |  |
| TNOM | Parameter measurement temperature | ${ }^{\circ} \mathrm{C}$ | 27 | 27 |  |  |  |  |  |
|  | PSPICE extensions |  |  |  |  |  |  |  |  |
| N | Gate pn emission coefficient | - | 1 | 1 |  |  |  |  |  |
| ISR | Gate pn recombination current parameter | A | 0 |  |  |  |  |  |  |
| NR | Emission coefficient for ISR | - | 2 | 2 |  |  |  |  |  |
| ALPHA | Ionization coefficient | $1 / \mathrm{V}$ | 0 |  |  |  |  |  |  |
| VK | Ionization "knee" voltage | V | 0 |  |  |  |  |  |  |
| M | Grading p-n coefficient | - | 0.5 | 0.5 |  |  |  |  |  |
| VTOTC | VTO temperature coefficient | $\mathrm{V} /{ }^{\circ} \mathrm{C}$ | 0 |  |  |  |  |  |  |
| BETACE | BETA exponential temperature <br> coefficient | $\% /{ }^{\circ} \mathrm{C}$ | 0 |  |  |  |  |  |  |
| XTI | IS temperature coefficient | - | 3 | 3 |  |  |  |  |  |

## Examples:

* JFET p-type, analog switch; 40 V 50 mA , low Ron resistance
.MODEL J175 PJF (VTO $=-5$ BETA=3.6m LAMBDA=7m RD=15 RS=15 IS=3.5f CGS=12P
$+\mathrm{CGD}=16 \mathrm{P}$ KF=5E-16)
* JFET n-type, analog switch; 40 V 50 mA , low Ron resistance
.MODEL 1N4393 NJF (VTO=-1.50 BETA=4m LAMBDA=. 035 RD=14 RS=15 IS=2E-15
+ CGS=7p CGD=9p KF=1.5E-16

```
* JFET n-type, low noise, very high frequency
.MODEL 1N4416 NJF (VTO=-3.8 BETA=5.3m LAMBDA=.035 RD=35 RS=100 IS=5.E-15
+CGS=6p CGD=3p KF=3.246E-18)
*JFET n-type, general purpose 25 V, 10 mA
.MODEL 1N5457 NJF (VTO=-3 BETA=1.5m LAMBDA=5.16m RD=40 RS=70 IS=5f
+CGS=15p CGD=4p KF=3E-17)
*JFET n-type, low-noise audio amplifier 30 V, 10 mA
.MODEL BC264B NJF VTO=-1.8 BETA=1.2m LAMBDA=18m RD=0 RS=0
+ IS = 0.3f CGS= p CGD=2p PB=0.77
```


## K - Mutual Coupling



| General forms | Restrictions |
| :---: | :---: |
| Kname Lnamel Lname2 Value |  |
| Kname Lname1 Lname2 ... Value [Model [size]] | PSPICE |
| Kname Tnamel Tname2 $\mathbf{C m}=$ Cap_coupl $\mathbf{L m}=$ Ind_coupl | PSPICE |
| Examples |  |
| K4 L5 L7 0.9 |  |
| KTUN L4 L 70.95 |  |
| K5 T1 T7 Cm= $10.0 \mathrm{pF} \mathbf{L m}=5 \mathrm{mH}$ | PSPICE |
| K12 L6 L8 L2 0.85 | PSPICE |
| K6 L2 L3 0.99 KMOD | PSPICE |

The mutual coupling statement describes a mutual inductive coupling between two inductors. Lname1 and Lname 2 are the names of the two coupled inductors, and Value is the coupling coefficient $K$ which must be greater than 0 and less than or equal to 1 . Using the dot convention, place a dot on the first node of each inductor. The relation between the coupling coefficient $K$ and the mutual inductance is given by:

$$
\begin{equation*}
M_{i j}=K \sqrt{L_{i} L_{j}} \tag{K-1}
\end{equation*}
$$

where $L_{i}$ and $L_{j}$ are the coupled pair of inductors, and $M_{i j}$ is the mutual inductance between $L_{i}$ and $L_{j}$
A voltage induced in ith inductor $L_{i}$ is given by:

$$
\begin{equation*}
v_{i}=L_{i} \frac{d I_{i}}{d t}+M_{i j} \frac{d I_{j}}{d t}+M_{i k} \frac{d I_{k}}{d t}+\cdots \tag{K-2}
\end{equation*}
$$

Newer versions of PSPICE include a model for inductive and capacitive coupling between two transmission lines using $\mathbf{L m}$ and $\mathbf{C m}$ coupling parameters. In the case of mutual coupling between transmission lines (names start with the letter $\mathbf{T}$ ), two parameters can be specified. The $\mathbf{C m}$ parameter describes the capacitive coupling in $\mathrm{F} / \mathrm{m}$, and the $\mathbf{L m}$ parameter describes inductive coupling in $\mathrm{H} / \mathrm{m}$. PSPICE allows for declaration of coupling between more than two inductors.

In PSPICE the CORE model can be used to model lossy transformers; see: D. C. Jiles and D. L. Atherton, "Theory of Ferromagnetic Hysteresis", Journal of Magnetism and Magnetic Materials 61, 48 (1986).. The following .MODEL statement can accompany the mutual coupling declaration.

## 1. Core model

.MODEL Model CORE [.MODEL name type [list_of_parameters] ...

## 2. Model parameters

| Name | Parameter | Units | Default |
| :---: | :--- | :---: | :---: |
| AREA | Mean magnetic cross section | $\mathrm{cm}^{2}$ | 0.1 |
| PATH | Mean magnetic path length | cm | 1 |
| GAP | Effective air-gap length | cm | 0 |
| PACK | Pack (stacking) factor |  | 1 |
| MS | Magnetization saturation | $\mathrm{A} / \mathrm{m}$ | $10^{+6}$ |
| A | Thermal energy parameter | $\mathrm{A} / \mathrm{m}$ | $10^{0^{3}}$ |
| C | Domain flexing parameter |  | 0.2 |
| K | Domain anisotropy parameter | $\mathrm{A} / \mathrm{m}$ | 500 |
| ALPHA | Interdomain coupling parameter |  | $10^{-3}$ |
| GAMMA | Domain damping parameter | $1 / \mathrm{s}$ |  |

L - Inductor


The inductor statement defines an inductor with inductance specified by Value (in H) where Pnode and Nnode are the positive and negative nodes. An optional statement IC=Init_cond specifies the initial (time-zero) current that flows from Pnode, through the inductor, to Nnode. This initial condition takes effect only when the UIC option is specified in the .TRAN statement.

In SPICE2, a nonlinear inductor can be defined using the POLY keyword where $c 0 c 1 c 2$ ... are the coefficients of a polynomial describing the element value. The inductance is expressed as a function of the current through the inductor and is computed as

$$
\begin{equation*}
\text { Value }=c 0+c 1 I+c 2 I^{2}+\ldots \tag{L-1}
\end{equation*}
$$

Although the nonlinear inductor was originally implemented in SPICE2 with the keyword POLY, very few newer SPICE versions have this option implemented.


| General forms | Restrictions |
| :---: | :---: |
| $\mathbf{M n a m e}$ Dnode Gnode Snode Bnode Model [ $\mathbf{L}=$ Length] [W=Width] <br> $+[\mathbf{A D}=$ Darea $][\mathbf{A S}=$ Sarea $][\mathbf{P D}=$ Dperi $][\mathbf{P S}=$ Speri $][\mathbf{N R D}=$ Dsq $]$ <br> $+[\mathbf{N R S}=S s q][\mathbf{O F F}][\mathbf{I C}=V d s, V g s, V b s]$ <br> $\mathbf{M n a m e}$ Dnode Gnode Snode Bnode Model [L=Length] [W=Width] <br> $+[\mathbf{A D}=$ Darea $][\mathbf{A S}=$ Sarea $][\mathbf{P D}=$ Dperi $][\mathbf{P S}=$ Speri $][\mathbf{N R D}=$ Dsq $]$ <br> $+[\mathbf{N R S}=S s q][\mathbf{N R G}=G s q][\mathbf{N R B}=B s q][\mathbf{M}=$ Value $]$ <br> Mname Dnode Gnode Snode Bnode Model [L=Length] [W=Width] <br> $+[\mathbf{A D}=$ Darea $][\mathbf{A S}=$ Sarea $][\mathbf{P D}=$ Dperi $][\mathbf{P S}=$ Speri $][\mathbf{N R D}=$ Dsq $]$ <br> $+[\mathbf{N R S}=S s q][\mathbf{O F F}][\mathbf{I C}=V d s, V g s, V b s][\mathbf{T E M P}=T]$ <br> Examples | PSPICE SPICE3 |
| M1 3790 PMOS L=5u W=20u <br> M7 126010 TYPEP <br> M12 101980 mosn w=5.6u l=67. 3u <br> M4 4620 MODN L=3u W=15u AD=200p AS=200pP PD=30u PS=40u <br> M78730 TYPEN <br> MA 4788 PNOM L=2.5u $\mathbf{W}=16 u$ <br> MB 36920 PNOM L=2.5u $\mathbf{W}=10 u \quad$ TEMP=55 <br> M4 4520 NMOD L=5u W=40u AD=150p AS=150p PD=40u <br> + PS=40u NRD=15 NRS=25 NRG=12 | SPICE3 PSPICE |

Mname is the device name, and in the case of the MOS transistor it must begin with the letter M. Dnode, Gnode, Snode, and Bnode are the drain, gate, source and bulk/substrate/well nodes, respectively. Model is the model name, and $\mathbf{L}$ and $\mathbf{W}$ are the channel length and width in meters. AD and $\mathbf{A S}$ are the drain and source diffusion areas in square meters. PD and $\mathbf{P S}$ are the perimeters of the drain and source lateral junctions in meters. NRD and NRS are the relative resistivities of the drain and source in number of squares. These parasitic resistances can be specified either by sheet resistance RSH, which is multiplied by NRD and NRS, or by RD and RS in the .MODEL definition. The calculation of resistance using the sheet resistance concept (resistance per square) is also explained in the resistor Section (Eq. R-1). Default values for $\mathbf{L}$, $\mathbf{W}, \mathbf{A D}$ and $\mathbf{A S}$ are $\mathbf{L}=100 \mu \mathrm{~m}, \mathbf{W}=100 \mu \mathrm{~m}, \mathbf{A D}=0$, and $\mathbf{A S}=0$. These default values can be changed with the .OPTION statement using DEFL, DEFW, DEFAS, and DEFAD keywords. Default values of PD and PS are 0.0, while default values of NRD and NRS are 1.0.

In SPICE2/3, the keyword OFF indicates an optional starting condition of the device for dc analysis. The optional initial value $\mathbf{I C}=V d s, V g s, V b s$ is used together with UIC in a transient
analysis. In the case of the SPICE3, the optional TEMP value is the temperature at which this device operates and it overrides the temperature specified in the .OPTION statement.

In PSPICE, in addition to source and drain resistances, the user may specify the gate and bulk resistances using NRG and NRB parameters. $\mathbf{M}$ is a device multiplier which simulates the effect of multiple transistors connected in parallel.

## 1. MOS transistor models

## .MODEL Model_name NMOS [Model parameters] <br> .MODEL Model_name PMOS [Model parameters]

A large number of MOS transistor models are used. These models are distinguished by the keyword LEVEL and a number. Some SPICE implementations (i.e. AIM-SPICE) have up to 20 different levels of MOS models. In this section three basic levels (1, 2, and 3), which are implemented in all SPICE versions, and the newer BSIM models, which are also becoming a standard, are described. Numbers in the brackets reefer to the reference list at the end of MOS section of Chapter 6.

LEVEL=1 Shichman-Hodges model [1] [8]
LEVEL=2 Geometric-based analytical Meyer model [2] [8]
LEVEL=3 Semi-empirical short channel Dang model [3] [8]
LEVEL $=4 \quad$ BSIM1 (Berkeley Short Channel Igfet Model) [4] [9]
LEVEL=5 BSIM2 Jeng model [5] [9]
LEVEL=5 BSIM3 (version 1) [6] [9]
LEVEL=6 BSIM3 (version 2) [6] [9]
LEVEL=6 MOS6 Sakurai-Newton model [7]

All SPICE implementations All SPICE implementations All SPICE implementations SPICE3 and new PSPICE

SPICE3
New PSPICE
New PSPICE
SPICE3
2. Parameters of MOS transistor models

| Common for all Levels |  |  |  |  |
| :---: | :--- | :---: | :---: | :---: |
| Name | Parameter description | Unit | Default | Typical |
| LEVEL | Model index | - | 1 |  |
| L | Default channel length (PSPICE only) | m | DEFL | $100 \mu$ |
| $\mathbf{W}$ | Default channel width (PSPICE only) | m | DEFL | $100 \mu$ |
| RD | Drain ohmic resistance | $\Omega$ | 0 | 5 |
| RS | Source ohmic resistance | $\Omega$ | 0 | 5 |
| RG | Gate ohmic resistance (PSPICE only) | $\Omega$ | 0 | 5 |
| RB | Bulk/substrate ohmic resistance (PSPICE only) | $\Omega$ | 0 | 5 |
| CBD | Zero-bias bulk-drain junction capacitance | F | 0 | 20 fF |
| $\mathbf{C B S}$ | Zero-bias bulk-source junction capacitance | F | 0 | 20 fF |


| IS | Bulk junction saturation current | A | $10^{-14}$ | $3 \cdot 10^{-15}$ |
| :---: | :---: | :---: | :---: | :---: |
| JS | Bulk junction saturation current per sq-meter of junction area | A/m ${ }^{2}$ | 0 | $10^{-8}$ |
| JSSW | Bulk junction saturation current per length of sidewall area (PSPICE only) | A/m | 0 | $10^{-12}$ |
| N | Bulk junction emission coefficient (PSPICE only) | - | 1 | 1 |
| PB | Bulk junction potential | V | 0.8 | 0.85 |
| PBSW | Bulk junction sidewall potential (PSPICE only) | V | PB | 0.85 |
| CGSO | Gate-source overlap capacitance per meter channel width | F/m | 0 | $3 \cdot 10^{-11}$ |
| CGDO | Gate-drain overlap capacitance per meter channel width | F/m | 0 | $3 \cdot 10^{-11}$ |
| CGBO | Gate-bulk overlap capacitance per meter channel length | F/m | 0 | $3 \cdot 10^{-10}$ |
| RSH | Drain and source diffusion sheet resistance | $\Omega /$ | 0 | 10 |
| CJ | Zero-bias bulk junction bottom capacitance per square meter of junction area | $\mathrm{F} / \mathrm{m}^{2}$ | 0 | $2 \cdot 10^{-4}$ |
| CJSW | Zero-bias bulk junction sidewall capacitance per length of sidewall | F/m | 0 | $10^{-8}$ |
| MJ | Bulk junction bottom grading coefficient | - | 0.5 | 0.5 |
| CJSW | Zero-bias bulk junction sidewall capacitance per meter of junction perimeter (PSPICE only) | F/m | 0 | $10^{-9}$ |
| MJSW | Bulk junction sidewall grading coefficient (PSPICE only) | - | $\begin{gathered} 0.50 \text { (Level 1) } \\ 0.33 \text { (Level 2, 3) } \end{gathered}$ |  |
| TT | Bulk junction transit time (PSPICE only) | s | 0 | $10^{-8}$ |
| KF | Flicker noise coefficient | - | 0 | $10^{-26}$ |
| AF | Flicker noise exponent | - | 1.0 | 1.2 |
| FC | Coefficient for forward-bias depletion capacitance formula | - | 0.5 | 0.5 |
| TNOM | Nominal temperature which overwrites the value specified in .OPTION statement (SPICE3 only) | K | 300 | 300 |

## Level 1, 2, 3, and 6 (Sakurai-Newton)

| Name | Parameter description | Unit | Default | Typical |
| :---: | :---: | :---: | :---: | :---: |
| VTO | Zero-bias threshold voltage | V | 0 | 1.0 |
| KP | Transconductance parameter | A/ $\mathrm{V}^{2}$ | $2 \cdot 10^{-5}$ | $3 \cdot 10^{-5}$ |
| GAMMA | Bulk threshold parameter | $\mathrm{V}^{0.5}$ | 0 | 0.35 |
| PHI | Surface potential | V | 0.6 | 0.65 |
| LAMBDA | Channel-length modulation parameter (level 1 and level 2 only) | 1/V | 0 | 0.02 |
| TOX | Oxide thickness | m | $10^{-7}$ | $10^{-7}$ |
| NSUB | Substrate doping | $\mathrm{cm}^{-3}$ | 0 | $5 \cdot 10^{15}$ |
| NSS | Surface state density | $\mathrm{cm}^{-2}$ | 0 | $2 \cdot 10^{10}$ |
| NFS | Fast surface state density | $\mathrm{cm}^{-2}$ | 0 | $10^{10}$ |
| TPG | Type of gate material (+1 for opposite to substrate, -1 for same as substrate, and 0 for Al gate) | - | 1 | 1 |
| XJ | Metallurgical junction depth | m |  | 1 u |
| LD | Lateral diffusion | m | 0 | 0.7u |
| WD | Lateral diffusion width (PSPICE only) | m | 0 | 0.5u |
| UO | Surface mobility | $\mathrm{cm}^{2} / \mathrm{V}-\mathrm{s}$ | 600 | 700 |
| UCRIT | Critical field for mobility degradation (level 2 only) | V/cm | $10^{4}$ | $10^{4}$ |
| UEXP | Critical field exponent in mobility degradation (level 2 only) | - | 0 | 0.1 |
| UTRA | Transverse field coefficient (mobility) (deleted for level 2) | - | 0 | 0.3 |
| VMAX | Maximum drift velocity of carriers | m/s | 0 | $3 \cdot 10^{4}$ |
| NEFF | Total channel charge (fixed and mobile) coefficient (level 2 only) | - | 1.0 | 3.0 |
| XQC | Thin-oxide capacitance model flag and a fraction of channel charge attributed to drain (0-0.5) | - | 1 | 0.4 |
| DELTA | Width effect on threshold voltage | - | 0 | 1.0 |
| THETA | Mobility modulation (level 3 only) | 1/V | 0 | 0.1 |
| ETA | Static feedback (level 3 only) | - | 0 | 1.0 |
| KAPP | Saturation field factor (level 3 only) | - | 0.2 | 0.5 |

Transistor parameters may often be specified in different ways. For example, the reverse current can be specified either with the IS parameter (in A) or with JS (in A/m²). The first choice is an absolute value, while the second choice is multiplied by $\mathbf{A D}$ and $\mathbf{A S}$ to give the reverse current at the drain and source junctions, respectively. The latter approach is preferred. The same is also true for the parameters CBD, CBS, and CJ. Parasitic resistances can be given with RD and RS (in $\Omega$ ) or with RSH (in $\Omega /$ ). RSH is multiplied by number of squares NRD and NRS.

## Examples:

```
* NMOS transistor for 2um n-well MOSIS technology
.MODEL CMOSN NMOS LEVEL=2 PHI=0.7 TOX=40n XJ=0.2U TPG=1 VTO=0.8
+ DELTA=4.1 LD=0.3u KP=45u UO=550 UEXP=0.12 UCRIT=96k RSH=0.15 GAMMA=0.6
+ NSUB=7.3E+15 NFS=1.1E+11 VMAX=59k LAMBDA=0.03 CGDO=400p CGSO=400p
+ CGBO=350p CJ=0.1m MJ=0.6 CJSW=470p MJSW=0.3 PB=0.8
* PMOS transistor for 2um n-well MOSIS technology
.MODEL CMOSP PMOS LEVEL=2 PHI=0.7 TOX=40n XJ=0.2U TPG=-1 VTO=-0.9
+ DELTA=4.6 LD=0.35u KP=17u UO=205 UEXP=0.29 UCRIT=83k RSH=0.11 GAMMA=0.7
+ NSUB=9.5E+15 NFS=1.1E+11 VMAX=1MEG LAMBDA=0.046 CGDO=440p
+ CGSO=440p CGBO=390p CJ=0.3m MJ=0.6 CJSW=280p MJSW=0.4 PB=0.8
```

In the case of BSIM parameters for LEVEL=4, there are no default values, and all parameters must be specified. Also, some parameters, those marked with an asterisk "*" in the Table for Level 4, have channel length/width dependencies. For each of these parameters, two additional parameters should be specified. For example, if a parameter has the name PNAM then two additional parameters LPNAM and WPNAM should be specified. The actual parameter value is calculated using

$$
\text { PNAM }=\text { PNAM }+\frac{\text { LPNAM }}{\text { L }- \text { DL }}+\frac{\text { WPNAM }}{\text { W }- \text { DW }}
$$

where $\mathbf{L}$ and $\mathbf{W}$ are the channel length and width specified in the device line. Level 4 parameters were designed for automatic parameter extraction, and all model parameters should be copied from the device extractor rather than entered manually.

| Level 4 - BSIM1 |  |  |  |
| :---: | :--- | :---: | :---: |
| Name | Parameter description | Unit | L/W |
| TOX | Gate oxide thickness | $\mu \mathrm{m}$ |  |
| VFB | Flat band voltage | V | $*$ |
| PHI | Surface inversion potential | V | $*$ |
| K1 | Body effect coefficient |  | $*$ |
| K2 | Drain/source depletion charge sharing coefficient | - | $*$ |


| DL | Shortening of channel | $\mu \mathrm{m}$ |  |
| :---: | :---: | :---: | :---: |
| DW | Narrowing of channel | $\mu \mathrm{m}$ |  |
| N0 | Zero-bias subthreshold slope coefficient | - | * |
| NB | Sensitivity of subthreshold slope to substrate bias | - | * |
| ND | Sensitivity of subthreshold slope to drain bias | - | * |
| VDD | Measurement bias range | V |  |
| MUS | Mobility at zero substrate bias and at $V_{D S}=$ VDD | $\mathrm{cm}^{2} / \mathrm{V} \cdot \mathrm{s}$ |  |
| X2MS | Sensitivity of mobility to substrate bias at $V_{D S}=$ VDD | $\mathrm{cm}^{2} / \mathrm{V}^{2} \cdot \mathrm{~s}$ | * |
| X3MS | Sensitivity of mobility to drain bias at $V_{D S}=$ VDD | $\mathrm{cm}^{2} / \mathrm{V}^{2} \cdot \mathrm{~s}$ | * |
| MUZ | Zero-bias mobility | $\mathrm{cm}^{2} / \mathrm{V} \cdot \mathrm{s}$ |  |
| X2MZ | Sensitivity of mobility to substrate bias at $V_{D S}=0$ | $\mathrm{cm}^{2} / \mathrm{V}^{2} \cdot \mathrm{~s}$ | * |
| U0 | Zero-bias transverse-field mobility degradation coefficient | 1/V | * |
| X2U0 | Sensitivity of transverse field mobility degradation effect to substrate bias | $1 / V^{2}$ | * |
| U1 | Zero-bias velocity saturation coefficient | $\mu \mathrm{m} / \mathrm{V}$ | * |
| X2U1 | Sensitivity of velocity saturation effect to substrate bias | $\mu \mathrm{m} / \mathrm{V}^{2}$ | * |
| X3U1 | Sensitivity of velocity saturation effect on drain bias at $V_{D S}=\mathbf{V D D}$ | $\mu \mathrm{m} / \mathrm{V}^{2}$ | * |
| WDF | Source-drain junction default width | m |  |
| DELL | Source-drain junction length reduction | m |  |
| TEMP | Temperature at which parameters are measured | ${ }^{\circ} \mathrm{C}$ |  |
| ETA | Zero-bias drain-induced barrier-lowering coefficient | - | * |
| X2E | Sensitivity of drain-induced barrier-lowering effect to substrate bias | 1/V | * |
| X3E | Sensitivity of drain-induced barrier-lowering effect to drain bias at $V_{D S}=$ VDD | 1/V | * |
| XPART | Gate-oxide capacitance charge model flag. XPART $=0$ selects a 40/60 drain/source partition of the gate charge in saturation, while XPART $=1$ selects a $0 / 100$ drain/source charge partition. | - |  |



General forms
Oname n1 n2 n3 n4 Model
Restrictions
(In PSPICE, lossy transmission lines use names which start with the letter $\mathbf{T}$ )

## Examples

O5 2070 lmod
SPICE3
O1573123 connection

## 1. LTRA model

.MODEL Model LTRA [list_of_parameters]
2. Model parameters

SPICE3 only

| Name | Parameter | Units | Default | Restricti <br> ons |
| :---: | :--- | :---: | :---: | :---: |
| $\mathbf{R}$ | Resistance/length. | $\Omega / \mathrm{m}$ | 0.0 | SPICE3 |
| $\mathbf{L}$ | Inductance/length. | $\mathrm{H} / \mathrm{m}$ | 0.0 | SPICE3 |
| $\mathbf{C}$ | Capacitance/length. | $\mathrm{F} / \mathrm{m}$ | 0.0 | SPICE3 |
| $\mathbf{G}$ | Conductance/length. | $1 / \Omega \cdot \mathrm{m}$ | 0.0 | SPICE3 |
| LEN | Length of line. | m | - | SPICE3 |
| REL | Breakpoint control. | - | 1 | SPICE3 |
| ABS | Breakpoint control. | 1 | SPICE3 |  |
| NOSTEPLIMIT | Don't limit time step to less than line <br> delay. This flag will remove the <br> default restrictions of limiting the <br> time-step to less than the line delay in <br> the RLC case. | Not set | SPICE3 |  |
| NOCONTROL | Don't do complex timestep control. <br> This flag prevents the default | Flag | Not set | SPICE3 |
|  | limitation on the time-step based on <br> convolution error criteria in the RLC <br> and $R C$ cases. This speeds up the <br> simulation, but may in some cases <br> reduce the accuracy. |  |  |  |


| LININTERP | Use linear interpolation. When this flag is set, linear interpolation is used instead of the default quadratic interpolation for calculating delayed signals. | Flag | Not set | SPICE3 |
| :---: | :---: | :---: | :---: | :---: |
| MIXEDINTERP | When this flag is set, SPICE uses a metric for judging whether quadratic interpolation is applicable, and if not so, it uses linear interpolation. Otherwise the default quadratic interpolation is used. | Flag | Not set | SPICE3 |
| COMPACTREL | Special RELTOL for history compacting | - | RELTOL | SPICE3 |
| COMPACTABS | Special ABSTOL for history compacting | - | ABSTOL | SPICE3 |
| TRUNCNR | Use Newton-Raphson method for time step control. This flag initiates Newton-Raphson iterations to determine an appropriate time step in the time step control routines. The default is a trial-and-error procedure which cuts the previous time step in half. | Flag | Not set | SPICE3 |
| TRUNCDONTCUT | Don't limit time step to keep impulseresponse errors low. This flag removes the default cutting of the time step to limit errors in the actual calculation of impulse-response related quantities. | Flag | Not set | SPICE3 |

## Example:

* coaxial cable with $\mathrm{Z} 0=50$ ohms and $100 \mathrm{pF} / \mathrm{m} 100 \mathrm{~m}$ long
.MODEL LOSSY LTRA(R=2.5 G=0 L=250n C=100P LEN=100)
LTRA uses a two-port convolution model for lossy transmission lines. $n 1$ and $n 2$ are the nodes at port 1 , and $n 3$ and $n 4$ are the nodes at port 2 . It is worth mentioning that a lossy transmission line with zero loss may be more accurate than the lossless transmission line. The length LEN of the line must be specified.

The following types of lines are implemented :

- $R L C$ - uniform transmission line with series loss only
- $R C$ - uniform $R C$ line
- $L C$ - lossless transmission line
- $R G$ - distributed series resistance and parallel conductance only

Other line structures may lead to erroneous results

|  |  |
| :---: | :---: |
| General forms | Restrictions |
| $\begin{aligned} & \text { Qname Cnode Bnode Enode }[\text { Snode }] \text { Model }[\text { Rarea }] \\ & \text { Qname Cnode Bnode Enode }[\text { Snode }] \text { Model }[\text { Rarea }][\text { OFF }][\text { IC=Vbe, Vce }] \\ & +[\mathbf{T E M P}=T] \end{aligned}$ | PSPICE <br> SPICE3 |
| Examples |  |
| Q3 4560 QMOD OFF <br> Q7 460 QMOD2 $\mathbf{I C}=0.7,10$ <br> Q12 479 QPNP <br> Q17 739 QNPN IC=0.6,5.0 TEMP=55 | SPICE3 |

Qname is the device name for a bipolar junction transistor and it must begin with the letter Q. Cnode, Bnode, Enode, and Snode are the collector, base, emitter and substrate nodes, respectively. For the case of NPN and PNP transistors, the substrate node is associated with the collector-substrate diode. For the case of LPNP (lateral pnp transistor) the substrate is associated with the base-substrate diode. If Snode is not given, ground is assumed. Model is the model name and Rarea is the relative area. If Rarea is omitted, the default Rarea=1.0 is assumed. The keyword OFF indicates an optional starting condition of the device for dc analysis. The optional initial value $\mathbf{I C}=V b e$, Vce is used together with UIC in transient analysis. In the case of the SPICE3, the optional TEMP value is the temperature at which this device operates, and it overrides the temperature specified In the .OPTION statement.

## 1. Bipolar transistor models

.MODEL Model_name NPN [Model parameters]
.MODEL Model_name PNP [Model parameters]
.MODEL Model_name LPNP [Model parameters]
PSPICE only
2. Parameters of bipolar transistor model (modified
Gummel-Poon model )

| Name | Parameter description | Unit | Default | Typical |
| :---: | :--- | :---: | :---: | :---: |
| IS | Saturation current for Rarea $=1$ | A | $10^{-16}$ | $10^{-15}$ |
| ISE | B- $E$ leakage saturation current for Rarea $=1$ | A | 0 | $10^{-12}$ |
| ICS | B-C leakage saturation current for Rarea $=1$ | A | 0 | $10^{-12}$ |
| BF | Forward current gain | - | 100 | 100 |


| BR | Reverse current gain | - | 1 | 0.1 |
| :---: | :---: | :---: | :---: | :---: |
| NF | Forward current emission coefficient | - | 1.0 | 1.2 |
| NR | Reverse current emission coefficient | - | 1.0 | 1.3 |
| NE | B-E leakage emission coefficient | - | 1.5 | 1.4 |
| NC | B-C leakage emission coefficient | - | 1.5 | 1.4 |
| VAF | Forward Early voltage | V | $\infty$ | 100 |
| VAR | Reverse Early voltage | V | $\infty$ | 50 |
| IKF | $\beta_{F}$ high current roll-off corner | A | $\infty$ | 0.05 |
| IKR | $\beta_{R}$ high current roll-off corner | A | $\infty$ | 0.01 |
| IRB | Current where base resistance falls by half for Rarea=1 | A | $\infty$ | 0.1 |
| RB | Zero-bias base resistance | $\Omega$ | 0 | 100 |
| RBM | Minimum base resistance | $\Omega$ | RB | 10 |
| RE | Emitter series resistance for Rarea=1 | $\Omega$ | 0 | 1 |
| RC | Collector series resistance for Rarea=1 | $\Omega$ | 0 | 50 |
| CJE | $B-E$ zero-bias depletion capacitance | F | 0 | $10^{-12}$ |
| CJC | $B-C$ zero-bias depletion capacitance | F | 0 | $10^{-12}$ |
| CJS | Zero-bias collector-substrate capacitance | F | 0 | $10^{-12}$ |
| VJE | $B-E$ built-in potential | V | 0.75 | 0.8 |
| VJC | $B$ - $C$ built-in potential | V | 0.75 | 0.7 |
| VJS | Substrate junction built-in potential | V | 0.75 | 0.7 |
| MJE | $B-E$ junction exponential factor | - | 0.33 | 0.33 |
| MJC | $B-C$ junction exponential factor | - | 0.33 | 0.5 |
| MJS | Substrate junction exponential factor | - | 0 | 0.5 |
| XCJC | Fraction of $B-C$ capacitance connected to internal base node (see Fig. 6) | - | 0 | 0.5 |
| TF | Forward transit time | s | 0 | $10^{-10}$ |
| TR | Reverse transit time | s | 0 | $10^{-8}$ |
| XTF | Coefficient for bias dependence of $\tau_{F}$ | - | 0 | - |
| VTF | Voltage for $\mathrm{t}_{F}$ dependence on $V_{B C}$ | V | $\infty$ | - |
| ITF | Current where $t_{F}=f\left(I_{C}, V_{B C}\right)$ starts | A | 0 | - |
| PTF | Excess phase at freq $=1 /\left(2 p t_{F}\right) \mathrm{Hz}$ | deg | 0 | - |
| XTB | Forward and reverse beta temperature exponent |  | 0 | - |


| EG | Energy gap | eV | 1.11 | 1.1 |
| :---: | :---: | :---: | :---: | :---: |
| XTI | Temperature exponent for effect on $I_{s}$ | - | 3 | 3.5 |
| KF | Flicker noise coefficient | - | 0 |  |
| AF | Flicker noise exponent | - | 1 |  |
| FC | Coefficient for the forward biased depletion capacitance formula | - | 0.5 | 0.5 |
| SPICE3 extension |  |  |  |  |
| TNOM | Nominal temperature which overrides the value specified in .OPTION statement | K | 300 | 300 |
| PSPICE extensions |  |  |  |  |
| NK | High-current roll-off coefficient | - | 0.5 | 0.5 |
| ISS | Substrate saturation current for Rarea=1 | A | 0 | $10^{-15}$ |
| NS | Substrate emission coefficient | - | 1 | 1 |
| QCO | Epitaxial layer charge factor for Rarea=1 | C | 0 |  |
| RCO | Epitaxial region resistance for Rarea=1 | $\Omega$ | 0 | 100 |
| VO | Carrier mobility knee voltage | V | 10 | 20 |
| GAMMA | Epitaxial layer doping factor |  | $10^{-11}$ | $10^{-11}$ |
| TRE1 | RE temperature coefficient (linear) | $1 /{ }^{\circ} \mathrm{C}$ | 0 | 0.001 |
| TRE2 | RE temperature coefficient (quadratic) | $1 /{ }^{\circ} \mathrm{C}^{2}$ | 0 | 0 |
| TRB1 | RB temperature coefficient (linear) | $1 /{ }^{\circ} \mathrm{C}$ | 0 | 0.002 |
| TRB2 | RB temperature coefficient (quadratic) | $1 /{ }^{\circ} \mathrm{C}^{2}$ | 0 | 0 |
| TRM1 | RBM temperature coefficient (linear) | $1 /{ }^{\circ} \mathrm{C}$ | 0 | 0.002 |
| TRM2 | RBM temperature coefficient (quadratic) | $1 /{ }^{\circ}{ }^{2}$ | 0 | 0 |
| TRC1 | $\mathbf{R C}$ temperature coefficient (linear) | $1 /{ }^{\circ} \mathrm{C}$ | 0 | 0.003 |
| TRC2 | RC temperature coefficient (quadratic) | $1 /{ }^{\circ} \mathrm{C}^{2}$ | 0 | 0 |

## Examples:

* small power general purpose npn transistor
.MODEL 2N2222 NPN (IS=15.2f NF=1 BF=105 VAF=98.5 IKF=.5 ISE=8.2p NE=2
$+\mathrm{BR}=4 \mathrm{NR}=1 \mathrm{VAR}=20 \mathrm{IKR}=.225 \mathrm{RE}=.373 \mathrm{RB}=1.49 \mathrm{RC}=.149 \mathrm{XTB}=1.5 \mathrm{CJE}=35.5 \mathrm{p}$
$+\mathrm{CJC}=12.2 \mathrm{P} \mathrm{TF}=0.5 \mathrm{n}$ TR=85n)
* small power general purpose pnp transistor $40 \mathrm{~V}, 200 \mathrm{~mA}$
.MODEL 2N2904 PNP (IS=0.3n NF=1 BF=100 VAF=120 IKF=. 14 ISE=46.1p NE=2 BR=4
$+\mathrm{NR}=1 \mathrm{VAR}=20 \mathrm{IKR}=.2 \mathrm{RE}=.5 \mathrm{RB}=2 \mathrm{RC}=.2 \mathrm{XTB}=1.5 \mathrm{CJE}=15 \mathrm{p} \mathrm{CJC}=20 \mathrm{p} \mathrm{TF}=600 \mathrm{p}$ TR=60n)

```
* small power general purpose npn transistor 40 V, 200 mA
.MODEL 2N3903 NPN (IS=1F NF=1 BF=400 VAF=120 IKF=70m ISE=3P NE=2 BR=4 NR=1
+ VAR=20 RE=21 RB=8 RC=1 XTB=1.5 CJE=8p CJC=5p TF=600p TR=0.3u)
*small power general purpose npn transistor 45 V, 200mA
.MODEL BC107A NPN (IS=10f NF=1 BF=300 VAF=120 IKF=0.05 ISE=5p NE=2 BR=4
+ NR=1 VAR=30 XTB=1.5 RE=1 RB=3 RC=0.3 CJE=15p CJC=5p TF=0.5n TR=60n)
*small power general purpose pnp transistor 45 V, 200 mA
.MODEL BC177A PNP (IS=0.1f ISE=0.5f NF=1 NE=1.4 BF=300 BR=13 IKF=.1 IKR=. 01
+ISC=0.1f NC=1.1 NR=1 RB=.2 RE=.4 RC=1 VAR=10 VAF=90 CJE=16p TF=.5n
+CJC=10p TR=70n MJC=.4 VJC=.6)
*small power germanium transistor 25 V, 100 mA
.MODEL 2N2955 PNP (IS=1.25n NF=1 BF=80 VAF=90 IKF=60m ISE=5n NE=2 BR=4 NR=1
+VAR=14 IKR=90m RE=2 RB=10 RC=1 XTB=1.5 CJE=30p CJC=9p TF=0.4n TR=20n)
* power npn transistor 15 A, 100V, 100 W
.MODEL 2N3055 NPN(IS=5p NF=1 BF=100 VAF=100 IKF=.25 ISE=30p ISC=5n RB=3
+IRB=1m RBM=.4 NE=1.5 RC=.04 BR=3 MJC=.4 VJE=1 MJE=.45 XTB=1 CJE=600p
+TF=80n CJC=200p TR=2u PTF=120 XTF=1 ITF=3)
* power npn transistor 4 A, 40 V
.MODEL 2N5190 NPN (IS=5p NF=1 BF=150 VAF=120 IKF=0.3 ISE=0.7n NE=2 BR=4
+ NR=1 VAR=20 XTB=2.5 RE=0.2 RB=12 RBM=1.2 IRB=0.5m RC=0.07 CJE=0.3n
+ CJC=0.3n TF=45n TR=1u PTF=120 XTF=1 ITF=3.5 ISC=5n MJC=0.2 VJC=1.2
+ MJE=0.3 VJE=0.5)
* power pnp transistor 4 A, 40 V
.MODEL 2N5193 PNP (IS=0.4p NF=1 BF=100 VAF=100 IKF=0.3 ISE=0.3n ISC=7n NE=2
+ BR=4 NR=1 VAR=20 XTB=1.4 RE=0.15 RB=15 RBM=1.5 IRB=0.3m RC=0.06 CJE=0.3n
+ CJC=0.5n VJC=1.25 MJE=0.3 VJE=0.65)
```



| General forms | Restrictions |
| :---: | :---: |
| Rname Pnode Nnode Value [TC=TC1 [TC2]] |  |
| Rname Pnode Nnode [ Value ] [Model] [L=Length] [W=Width] $+[$ TEMP $=T]$ | SPICE3 |
| Rname Pnode Nnode [Model] [ Value ] [TC=TC1 [TC2]] | PSPICE |
| Examples |  |
| R1371k |  |
| RC 79 10k TC=0.02,0.0015 |  |
| RL 393.7 k |  |
| RLOAD 212 RMODEL $\mathbf{L}=48 \mathrm{um} \mathbf{W}=3 \mathrm{um}$ | SPICE3 |
| R12 29 RMOD 800k TC = 0.01, 0.0015 | PSPICE |

The resistor statement consists of a name which must start with the letter $\mathbf{R}$, node names Pnode and Nnode, and a value of resistance specified by Value (in ohms). An ptional TC=TC1 [TC2]] specifies the temperature dependence of resistance, where $T C 1$ and $T C 2$ are linear and quadratic temperature coefficients, respectively.

The basic resistor statement has many extensions that are implementation-dependent. Semiconductor resistors are implemented in SPICE3. This extension models temperature effects and calculates the resistance based on geometry and processing information. If Value is given, then the Value defines the resistance, and information on geometry and processing is ignored. If Model is specified, the resistance value is calculated based on information about the process and geometry in the model statement:

$$
\begin{equation*}
R=\mathbf{R S H} \frac{\text { Length }- \text { NARROW }}{\text { Width }- \text { NARROW }} \tag{R-1}
\end{equation*}
$$

If Value is not given, Model and Length must be specified. If Width is not given, it will be given the default value. The optional TEMP value is the temperature at which this device operates. It overrides the default temperature specified in the .OPTION statement. The temperature dependence of the resistance is calculated using

$$
\begin{equation*}
R(T)=R(\mathbf{T N O M})\left[1+T C 1(T-\mathrm{TNOM})+T C 2(T-\mathrm{TNOM})^{2}\right] \tag{R-2}
\end{equation*}
$$

The resistor model contains process-related parameters, and the resistance value is a function of the temperature.

## 1. Resistor model

.MODEL Model $\mathbf{R}$ [list_of_parameters]
2. Model parameters

| Name | Parameter | Units | Default | Restrictions |
| :---: | :--- | :---: | :---: | :---: |
| TC1 | First-order temperature coefficient | $1 /{ }^{\circ} \mathrm{C}$ | 0.0 |  |
| TC2 | Second order temperature coefficient | $1 /{ }^{\circ} \mathrm{C}^{2}$ | 0.0 |  |
| RSH | Sheet resistance | $\Omega /$ | - | SPICE3 |
| DEFW | Default width | m | $1 \mathrm{e}-6$ | SPICE3 |
| NARROW | Narrowing due to side etching | m | 0.0 | SPICE3 |
| TNOM | Parameter measurement temperature | ${ }^{\circ} \mathrm{C}$ | 27 | SPICE3 |
| R | Resistance multiplier | - | 1 | PSPICE |
| TCE | Exponential temperature coefficient | $\% /{ }^{\circ} \mathrm{C}$ | 0 | PSPICE |

PSPICE uses the TCE parameter to calculate the temperature dependence of resistance:

$$
\begin{equation*}
R(T)=R\left(T_{\text {nom }}\right) 1.01^{\mathrm{TCE}\left(T-T_{\text {nom }}\right)} \tag{R-3}
\end{equation*}
$$

## S - Voltage Controlled Switch



| General forms | Restrictions |
| :--- | :---: |
| Sname Pnode Nnode Pinp Ninp Model | PSPICE |
| Sname Pnode Nnode Pinp Ninp Model [ON] [OFF] | SPICE3 |
|  |  |
| Sxamples |  |
| SW5 2 9 SW1 3 0 Smodel |  |
| S44962 SW2 OFF |  |
| S33729 sw1 ON | SPICE3 |
| s3 3680 SMOD off | SPICE3 |
|  | SPICE3 |

The voltage-controlled switch statement begins with the letter S. Pnode and Nnode represent the connections to the switch terminals. Pinp and Ninp are positive end negative controlling nodes, respectively. The model name, Model, is mandatory, while the initial conditions are optional. The controlling voltages are defined the same way as in voltage-controlled voltage (letter $\mathbf{E}$ ) and current (letter $\mathbf{G}$ ) sources. In SPICE3, the optional parameter ON or OFF specifies the switch state for the dc operating point.

The switch model allows an almost ideal switch to be described in SPICE. The switch is not quite ideal, in that the resistance cannot change from 0 to infinity, but must always have a finite and nonzero positive value. By proper selection of the on and off resistances, they can be effectively zero and infinity in comparison to other circuit elements.

The switch can have a hysteresis described by the VH parameter. For example, the voltagecontrolled switch will be in the on state, with a resistance RON, at VT+VH. The switch will be in the off state, with a resistance ROFF, at VT-VH.

## 1. SW model

.MODEL Model SW [list_of_parameters]
SPICE3

## 2. SW model parameters

| Name | Parameter | Default | Units | Restrictions |
| :---: | :--- | :---: | :---: | :---: |
| VT | Threshold voltage | 0.0 | V | SPICE3 |
| VH | Hysteresis voltage | 0.0 | V | SPICE3 |
| RON | On resistance | 1.0 | $\Omega$ |  |
| ROFF | Off resistance | $1 / \mathbf{G M I N}$ | $\Omega$ | SPICE3 |

Examples:
.MODEL SMOD SW RON=1m ROFF=20k VT=3V
.MODEL SMOD SW VT=4V VH=1V
.MODEL SMOD SW RON=10 ROFF=10MEG VT=2V
3. VSWITCH model
.MODEL Model VSWITCH [list_of_parameters]
PSPICE

## 4. VSWITCH model parameters

| Name | Parameter | Default | Units | Restrictions |
| :---: | :--- | :---: | :---: | :---: |
| VON | Threshold current for on state | $10^{-3}$ | V | PSPICE |
| VOFF | Threshold current for off state | 0.0 | V | PSPICE |
| RON | On resistance | 1.0 | $\Omega$ |  |
| ROFF | Off resistance | $10^{6}$ | $\Omega$ | PSPICE |

The use of an ideal element that is highly non-linear, such as a switch, can cause large discontinuities to occur in the circuit node voltages. The rapid voltage change associated with a switch changing state can cause numerical round off or tolerance problems leading to erroneous results or time step difficulties. You can improve the situation by taking the following steps. Set the switch impedances only high and low enough to be negligible with respect to other elements in the circuit. Using switch impedances that are close to "ideal" under all circumstances will aggravate the discontinuity problem. When modeling real devices such as MOSFETS, the on resistance should be adjusted to a realistic level depending on the size of the device being modeled.

If a wide range of ON to OFF resistance must be used (ROFF/RON $>10^{+12}$ ), then the tolerance on errors allowed during transient analysis should be decreased by specifying the .OPTIONS TRTOL parameter to be less than the default value of 7.0. When switches are placed around capacitors, the .OPTIONS CHGTOL parameters should also be reduced. Suggested values for these two options are 1.0 and 1E-16, respectively. These changes inform SPICE to be more careful near the switch points so that no errors are made due to the rapid change in the circuit response.

## T - Transmission Lines



$n 1$ and $n 2$ are the nodes at port $1 ; n 3$ and $n 4$ are the nodes at port 2 . For the ideal case, $\mathbf{Z 0}$ is the characteristic impedance. The transmission line's length can be specified either by TD, a delay in seconds, or by $\mathbf{F}$ and $\mathbf{N L}$, a frequency and a relative wavelength at $\mathbf{F}$. NL defaults to 0.25 ( $\mathbf{F}$ is then the quarter-wave frequency). Although TD and $\mathbf{F}$ are both shown as optional, one of the two must be specified.

Note that this element models only one propagating mode. If all four nodes are distinct in the actual circuit, then two modes may be excited. To simulate such a situation, two transmission-line elements are required. The (optional) initial condition specification consists of the voltage and current at each of the transmission line ports. Note that the initial conditions (if any) apply 'only' if the UIC option is specified on the .TRAN line. One should be aware that SPICE will use a transient time step which does not exceed $1 / 2$ the minimum transmission line delay. Therefore, very short transmission lines (compared with the analysis time frame) will cause long run times.

For the case of a lossy line, $\mathbf{L E N}$ is the electrical length. $\mathbf{R}, \mathbf{L}, \mathbf{G}$, and $\mathbf{C}$ are the per unit length values of resistance, inductance, conductance, and capacitance, respectively. The lossy line model is similar to that shown for the ideal case, except that the delayed voltage and current values include terms that vary with frequency. These terms are computed in transient analysis using an impulse response convolution method, and the internal time step is limited by the time resolution required to accurately model the frequency characteristics of the line. As with ideal lines, short lossy lines will cause long run times.

For the case of a line that uses a model, the electrical length is given after the model name. All of the transmission line parameters from either the ideal, or lossy parameter set can be expressions. In addition, $\mathbf{R}$ and $\mathbf{G}$ can be general Laplace expressions. This option allows the user to model frequency-dependent effects, such as skin effect and dielectric loss. However, this adds to the computation time for transient analysis, since the impulse responses must be obtained by an inverse FFT.

The simulator uses a distributed model to represent the properties of a lossy transmission line, and the line resistance, inductance, conductance, and capacitance are all continuously apportioned along the line's length. A common approach to simulating lossy lines is to model these characteristics using discrete passive elements to represent small sections of the line. This is the lumped model approach, which involves connecting a set of many small subcircuits in series.

An additional PSPICE extension allows systems of coupled transmission lines to be simulated. Transmission line coupling is specified using the $\mathbf{K}$ mutual coupling device. This is done in much the same way that coupling is specified for inductors.

The distributed model used in the simulation process frees you from having to determine how many lumps are sufficient, and eliminates spurious oscillations. It also allows lossy lines to be simulated in a fraction of the time necessary when using the lumped approach, for the same accuracy.

## 1. TRN model

.MODEL Model TRN [list_of_parameters]
2. Model parameters

PSPICE only

| Name | Parameter | Units | Default | Restrictions |  |
| :---: | :--- | :---: | :---: | :---: | :---: |
| Ideal transmission line |  |  |  |  |  |
| ZO | Characteristic impedance | $\Omega$ |  | PSPICE |  |
| TD | Transmission delay | s |  | PSPICE |  |
| NL | Relative wavelength |  | 0.25 | PSPICE |  |
| F | Frequency for NL | Hz |  | PSPICE |  |
|  |  |  |  |  |  |
| LENsy transmission line | Electrical length | Any unit |  | PSPICE |  |
| R | Resistance per LEN units | $\Omega /$ unit |  | PSPICE |  |
| L | Inductance per LEN unit | H/unit |  | PSPICE |  |
| C | Capacitance per LEN unit | F/unit |  | PSPICE |  |
| G | Conductance per LEN unit | $1 / \Omega \cdot$ unit |  | PSPICE |  |


$n 1$ and $n 2$ are the two nodes of the $R C$ line itself, while $n 3$ is the capacitive node. Model is the name of the model, Length is the length of the line in meters and Lumps, if given, is the number of segments to use in modeling the RC line.

## 1. URC model

.MODEL Model URC [list_of_parameters]
2. Model parameters SPICE3 only

| Name | Parameter | Units | Default | Restricti <br> ons |
| :---: | :--- | :---: | :---: | :---: |
| K | Propagation constant | - | 2.0 | SPICE3 |
| FMAX | Maximum frequency | Hz | $10^{9}$ | SPICE3 |
| RPERL | Resistance per unit length | $\Omega / \mathrm{m}$ | 1000 | SPICE3 |
| CPERL | Capacitance per unit length | $\mathrm{F} / \mathrm{m}$ | $10^{-15}$ | SPICE3 |
| ISPERL | Saturation current per unit length | $\mathrm{A} / \mathrm{m}$ | 0 | SPICE3 |
| RSPERL | Diode resistance per unit length | $\Omega / \mathrm{m}$ | 0 | SPICE3 |

The model is accomplished by a subcircuit expansion of the URC line into a network of lumped $R C$ segments with internally generated nodes. The $R C$ segments are in a geometric progression, increasing toward the middle of the URC line, with $\mathbf{K}$ as a proportionality constant. $\mathbf{N}$ is the number of lumped segments used. If not specified on the URC line, $\mathbf{N}$ is determined by the following expression:

$$
\begin{equation*}
\mathbf{N}=\frac{\log \left[2 \pi R C F_{\max }\left(\frac{\mathbf{K}-1}{\mathbf{K}}\right)^{2}\right]}{\log \mathbf{K}} \tag{U-1}
\end{equation*}
$$

The URC line is made up strictly of resistor and capacitor segments unless the ISPERL parameter is given a nonzero value, in which case the capacitors are replaced with reverse-biased diodes with a zero-bias junction capacitance equivalent to the capacitance replaced, and with a
saturation current of ISPERL amps per meter of transmission line. An optional series resistance equivalent to RSPERL ohms per meter can be included.

## V - Independent Voltage Source



| General forms | Restrictions |
| :---: | :---: |
| Vname Pnode Nnode [[DC] Value] [[AC] Mag [Phase]] [Signal_shape] |  |
| Vname Pnode Nnode [[DC] Value] [[AC] Mag [Phase]] | PSPICE |
| + [STIMULUS = Name ] [Signal_shape] |  |
| Vname Pnode Nnode [[DC] Value] [[AC] Mag [Phase]] [Signal_shape] <br> + [DISTOF1 F1mag [F1phase]] [DISTOF2 F2mag [F2phase]] | SPICE3 |
| Examples |  |
| VSC 26 AC 1 mV 45.0 |  |
| VNP 47 DC 3V AC 1mV 90.0 |  |
| VPULSE 30 PULSE (0 5.2V 5ns 1ns 1ns 30ns 50ns) |  |
| V620 DC 1V AC 1 mV SIN(0 0.001 1MEG) | PSPICE |
| V2 50 AC 10mV DISTOF1 DISTOF2 0.001 | SPICE3 |
| V3 69 AC 0.145 SFFM (0 1250 kHz 0.53 kHz ) | SPICE3 |

Value is the dc and transient analysis value of the voltage source. If the source value is time-invariant (e.g., a power supply), then the value may optionally be preceded by the letters DC.

Mag is the ac magnitude and Phase is the ac phase. The source is set to this value in the ac analysis. If Mag is omitted following the keyword $\mathbf{A C}$, a value of unity is assumed. If Phase is omitted, a value of zero is assumed. If parameters other than source values are omitted or set to zero, the default values shown will be assumed. If a source is assigned a time-dependent value, the time-zero value will be used for dc analysis.

The keyword STIMULUS is used in newer versions of PSPICE to call up custom signal shapes created with the stimulus editor. By specifying Signal_shape, a time-dependent waveform for transient analysis can be assigned. If a source is assigned a time-dependent value, the time-zero value is used for dc analysis. There are five independent source functions: pulse, exponential, sinusoidal, piecewise linear, and single-frequency FM. These five signal shapes are described in more detail in what follows.

## 1. Pulse waveforms

Form
PULSE (V1 V2 TD TR TF PW PER )
Examples: VIN 30 PULSE(0 5V 10us 2us 2us 50us 100us)
VIN 50 PULSE(-5V 5V 10us 2us 2us 50us)

| Parameters | Meaning | Default | Units |
| :---: | :--- | :---: | :---: |
| V1 | Initial value | - | V |
| V2 | Pulsed value | - | V |
| TD | Delay time | 0.0 | sec |
| TR | Rise time | Tstep | sec |
| TF | Fall time | Tstep | sec |
| PW | Pulse width | Tstop | sec |
| PER | Period | Tstop | sec |

Parameters Tstep and Tstop are specified in .TRAN statement.


## 2. Sine waves

Form SIN(VO VA FREQ TD DF PHASE)

Examples: V3 30 SIN(1V 2V 10MEG 1ns 1MEG) V6 62 SIN(0 10mV 100kHz)

| parameters | meaning | default | units | Restrictions |
| :---: | :--- | :---: | :---: | :---: |
| VO | Offset |  | V |  |
| VA | Amplitude |  | V |  |
| FREQ | Frequency | $1 /$ Tstop | Hz |  |
| TD | Delay | 0.0 | s |  |
| DF | Damping factor | 0.0 | $1 / \mathrm{s}$ |  |
| PHASE | Phase | 0.0 | degre <br> e | PSPICE |



The shape of the waveform is described by the following equations:
For time < TD:
$\mathbf{V O}+\mathbf{V A} \sin \left[2 \pi\left(\frac{\text { PHASE }}{360}\right)\right]$
For time > TD:
$\mathbf{V O}+\mathbf{V A} \exp [-($ time $-\mathbf{T D}) \mathbf{T H E T A}] \sin \left[2 \pi\left(\right.\right.$ FREQ $($ time $\left.\left.-\mathbf{T D})+\frac{\text { PHASE }}{360}\right)\right]$

## 3. Exponential waveforms

Format
$\operatorname{EXP}(\mathrm{V} 1 \mathrm{~V} 2 \mathrm{TD} 1$ TAU1 TD2 TAU2)
Examples: V3 $50 \mathbf{E X P}(-5-3$ 5ns 20ns 30ns 30ns)
V6 $32 \operatorname{EXP}(05$ 5ns 20ns)

| Parameters | Meaning | Default | Units |
| :---: | :--- | :---: | :---: |
| V1 | Initial value |  | V |
| V2 | Pulsed value |  | V |
| TD1 | Rise delay time | 0.0 | s |
| TAU1 | Rise time constant | Tstep | s |
| TD2 | Fall delay time | TD1+Tstep | s |
| TAU2 | Fall time constant | Tstep | s |



The shape of the waveform is described by the following equations:
For time < TD1

$$
\begin{equation*}
v(\text { time })=0 \tag{V-4}
\end{equation*}
$$

For TD1 < time < TD2

$$
\begin{equation*}
v(\text { time })=\mathbf{V} 1+(\mathbf{V} 2-\mathbf{V} 1)\left[1-\exp \left(-\frac{\text { time }-\mathbf{T D} 1}{\mathbf{T A U 1}}\right)\right] \tag{V-5}
\end{equation*}
$$

for time > TD2

$$
v(\text { time })=\mathbf{V} 1+(\mathbf{V} 2-\mathbf{V} 1)\left[1-\exp \left(-\frac{\text { time }-\mathbf{T D 1}}{\mathbf{T A U 1}}\right)\right]+(\mathbf{V} 1-\mathbf{V} 2)\left[1-\exp \left(-\frac{\text { time }-\mathbf{T D} 2}{\mathbf{T A U 2}}\right)\right](\mathbf{V}-\mathbf{6})
$$

## 4. Piecewise linear waveforms

Format: $\quad$ PWL(T1 V1 [Tn Vn ] ...)
Examples: V5 $37 \mathrm{PWL}(0-7 \mathrm{~V}$ 5us -7 V 6us 5V 20us 5V 21us -7 V 30us -8 V )
V3 42 PWL(5ms 5V 20ms 5V 30ms 0V )

| Parameters | Meaning | Default | Units |
| :---: | :---: | :---: | :---: |
| Tn | Time at corner | - | s |
| Vn | Voltage at corner | - | V |

Each pair of values $(\mathbf{T n}, \mathbf{V n})$ specifies the value of the source $\mathbf{V n}([i n \mathrm{~V})$ at time $=\mathbf{T n}$. The value of the source at intermediate values of time is determined by using linear interpolation of the input values.


## 5. FM waveforms

Form
SFFM(VO VA FC MDI FS)
Examples:

> V7 70 SFFM(0 1mV 20kHz 51 kHz )
> V1 120 SFFM(0 10V 300 kHz 0.510 kHz$)$

| parameters | meaning | default | units |
| :---: | :--- | :---: | :---: |
| VO | Offset | - | V |
| VA | Amplitude | - | V |
| FC | Carrier frequency | 1/Tstop | Hz |
| MDI | Modulation index | 0 |  |
| FS | Signal frequency | 1/Tstop | Hz |



The SFFM (single-frequency frequency-modulated) waveform is described by the following equation:

$$
\begin{equation*}
v(\text { time })=\mathbf{V O}+\mathbf{V A} \sin [2 \pi \mathbf{F C} \text { time }+\mathbf{M D I} \sin (2 \pi \mathbf{F S} \text { time })] \tag{V-7}
\end{equation*}
$$

## W - Current-Controlled Switch



| General forms | Restrictions |
| :--- | :---: |
| Wname Pnode Nnode Vname model | PSPICE |
| Wname Pnode Nnode Vname model [ON] [OFF] | SPICE3 |
|  |  |
| W3 4 7 VIN WMOD |  |
| WON 4 7 VON WRELAY |  |
| w1 4 0 vclock Switch |  |
| W2 5 2 VR SM1 ON | SPICE3 |
| wreset 72 V5 Lossysw OFF | SPICE3 |

The name of a current-controlled switch begins with the letter W. Pnode and Nnode represent the connections to the switch terminals. The model name, Model, is mandatory, while the initial conditions are optional. The controlling current is the current through the specified voltage source, defined the same way as in current-controlled dependent voltage (letter $\mathbf{F}$ ) and current (letter $\mathbf{H}$ ) sources. In SPICE3 the optional parameter ON or OFF specifies the switch state for the dc operating point.

The switch model allows an almost ideal switch to be described in SPICE. The switch is not quite ideal, in that the resistance cannot change from 0 to infinity, but must always have a finite and nonzero positive value. By proper selection of the on and off resistances, they can be effectively zero and infinity in comparison to other circuit elements.

The switch can have a hysteresis described by the $\mathbf{I H}$ parameter. For example, the currentcontrolled switch will be in the on state, with a resistance $\mathbf{R O N}$, at $\mathbf{I T}+\mathbf{I H}$. The switch will be in the off state, with a resistance ROFF, at IT-IH.

## 1. CSW model

.MODEL Model CSW [list_of_parameters]
SPICE3

## 2. Model parameters

| Name | Parameter | Default | Units | Restrictions |
| :---: | :--- | :---: | :---: | :---: |
| IT | Threshold current | 0.0 | A | SPICE3 |
| IH | Hysteresis current | 0.0 | A | SPICE3 |
| RON | On resistance | 1.0 | $\Omega$ |  |
| ROFF | Off resistance | $1 /$ GMIN | $\Omega$ | SPICE3 |

## Examples:

.MODEL SMOD CSW IT=3V IH=1V
.MODEL SMOD CSW RON=50 ROFF=10MEG IT=3mA
.MODEL Model ISWITCH [list_of_parameters]
PSPICE

## Model Parameters

| Name | Parameter | Default | Units | Restrictions |
| :---: | :--- | :---: | :---: | :---: |
| ION | Threshold current for on state | $10^{-3}$ | A | PSPICE |
| IOFF | Threshold current for off state | 0.0 | A | PSPICE |
| RON | On resistance | 1.0 | $\Omega$ |  |
| ROFF | Off resistance | $10^{6}$ | $\Omega$ | PSPICE |

The use of an ideal element that is highly nonlinear, such as a switch, can cause large discontinuities to occur in the circuit node voltages. The rapid voltage change associated with a switch changing state can cause numerical round off or tolerance problems leading to erroneous results or time step difficulties.

You can improve the situation by taking the following steps: Set the switch impedances only high and low enough to be negligible with respect to other elements in the circuit. Using switch impedances that are close to "ideal" under all circumstances will aggravate the discontinuity problem. When modeling real devices such as MOSFETS, the on resistance should be adjusted to a realistic level depending on the size of the device being modeled.

If a wide range of ON to OFF resistance must be used (ROFF/RON $>10^{+12}$ ), then the tolerance on errors allowed during the transient analysis should be decreased by specifying the .OPTIONS TRTOL parameter to be less than the default value of 7.0. When switches are placed around capacitors, the .OPTIONS CHGTOL parameters should also be reduced. Suggested values for these two options are 1.0 and $1 \mathrm{E}-16$, respectively. These changes inform SPICE to be more careful near the switch points so that no errors are made due to the rapid change in the circuit response.

## X - Subcircuit Calls



Subcircuits are specified in SPICE by using pseudo-elements beginning with the letter $\mathbf{X}$, followed by the circuit nodes $n 1$ [ $n 2 n 3 \ldots$...] to be used in expanding the subcircuit and the name Subname of the subcircuit. The subcircuit is defined by the .SUBCKT statement. The number of nodes in the subcircuit call ( $\mathbf{X}$ statement) must be the same as in the subcircuit declaration (.SUBCKT).

| Z - MESFET | SPICE3 only |
| :---: | :---: |
| NMF PMF |  |
|  |  |
| General forms | Restrictions |
| Zname Dnode Gnode Snode Model [Rarea] [OFF] [IC=Vds, Vgs] | SPICE3 |
| Examples |  |
| Z25 30 ZPMOD OFF | SPICE3 |
| Z7 632 ZNMO IC= 5.0, 1.0 | SPICE3 |

A MESFET is described by a statement starting with name of the MESFET device Zname. This name must start with the letter Z. Node numbers Dnode, Gnode, and Snode for drain, gate, and source follow the name. Next, the model name Model is listed. Model parameters are specified in the .MODEL statement. The keywords NMF and PMW are used there for $n$ channel and $p$-channel respectively. Rarea is the relative area factor. If Rarea is not specified, 1 is assumed. An optional parameter $\mathbf{I C}=V d$ is used together with a UIC in transient analysis. The keyword OFF indicates an optional starting condition for dc analysis.

## 1. MESFET models

## .MODEL Model_name NMF [Model parameters] .MODEL Model_name PMF [Model parameters]

## 2. Model parameters

| Name | Parameter | Units | Default | Typical | Rarea |
| :---: | :--- | :---: | :---: | :---: | :---: |
| VTO | Pinch-off voltage | V | -2.0 | -2.0 |  |
| BETA | Transconductance parameter | $\mathrm{A} / \mathrm{V}$ | $1.0 \mathrm{e}-4$ | $1.0 \mathrm{e}-3$ | $*$ |
| B | Doping tail extending parameter | $1 / \mathrm{V}$ | 0.3 | 0.3 | $*$ |
| ALPHA | Saturation voltage parameter | $1 / \mathrm{V}$ | 2 | 2 | $*$ |
| LAMBDA | Channel-length modulation parameter | $1 / \mathrm{V}$ | 0 | $1.0 \mathrm{e}-4$ |  |
| RD | Drain ohmic resistance | $\Omega$ | 0 | 100 | $*$ |
| RS | Source ohmic resistance | $\Omega$ | 0 | 100 | $*$ |
| CGS | Zero-bias $G$-S junction capacitance | F | 0 | 5 pF | $*$ |
| CGD | Zero-bias $G-D$ junction capacitance | F | 0 | 5 pF | $*$ |
| PB | Gate junction potential | V | 1 | 0.6 |  |
| KF | Flicker noise coefficient | - | 0 | - |  |
| AF | Flicker noise exponent | - | 1 | - |  |
| FC | Coefficient for forward-bias depletion <br> capacitance formula | - | 0.5 | - |  |

Asterisks in the last column indicates that this parameter in all equations is multiplied by Rarea parameter specified in the $\mathbf{Z}$ device line.

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