

# Polynomial Coefficient Based DC Testing of Non-Linear Analog Circuits

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## Analog Circuit Testing

To determine catastrophic (open or short) faults and fractional deviations in circuit components from their nominal values.

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## This Work

To propose a method to detect fractional deviations of circuit components from their nominal values in a large class of circuits.

# Outline

- 1 Motivation
- 2 Our Idea
- 3 Generalization
- 4 Results
- 5 Fault Diagnosis
- 6 Conclusion

# Motivation

## To Develop an Analog Circuit Test Scheme

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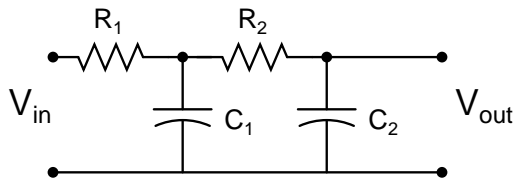
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# Previous Approaches

## Important Previous Techniques

- Signal flow graph – Complexity order is high [Bushnell et. al. '96]
- $I_{DDQ}$  based test – Intrusive, Area overhead is high [Chakravarty '97]
- **Transfer function based test** – Valid only for LTI systems [Savir et. al. '03]

# Transfer Function Coefficient - Based Test



Second order low pass filter

$$H(s) = \frac{1}{(R_1 R_2 C_1 C_2) s^2 + (R_1 C_1 + (R_1 + R_2) C_2) s + 1}$$

# Our Idea

Taylor series expansion of circuit function about  $v_{in} = 0$

$$V_{out} = f(v_{in})$$

$$V_{out} = f(0) + \frac{f'(0)}{1!} v_{in} + \frac{f''(0)}{2!} v_{in}^2 + \frac{f'''(0)}{3!} v_{in}^3 + \cdots + \frac{f^{(n)}(0)}{n!} v_{in}^n + \cdots$$

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Ignoring the higher order terms we have

$$v_{out} \approx a_0 + a_1 v_{in} + a_2 v_{in}^2 + \cdots + a_n v_{in}^n$$

where every  $a_i \in \mathfrak{R}$  and is bounded between its extreme values for

$$a_{i,\min} < a_i < a_{i,\max} \quad \forall i \quad 0 \leq i \leq n$$

# Our Idea (Contd..)

## In a Nutshell

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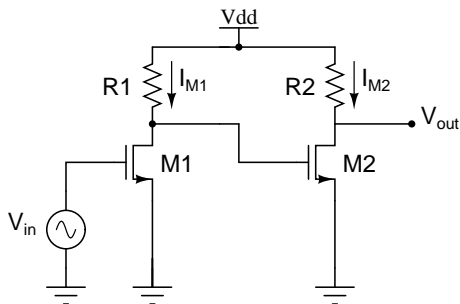
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- Find the  $V_{\text{out}}$  v/s  $V_{\text{in}}$  relationship at DC
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- Repeat the same for CUT by curve fitting the I/O response
- Compare each of the obtained coefficients with fault-free circuit range
- Classify CUT as **Good** or **Bad**

# Cascaded Amplifiers



Two stage amplifier with 4<sup>th</sup> degree non-linearity in  $V_{in}$

$$v_{out} = a_0 + a_1 v_{in} + a_2 v_{in}^2 + a_3 v_{in}^3 + a_4 v_{in}^4$$

# Polynomial Coefficients

$$a_0 = V_{DD} - R_2 K \left( \frac{W}{L} \right)_2 \left[ \begin{array}{l} (V_{DD} - V_T)^2 + R_1^2 K^2 \left( \frac{W}{L} \right)_1^2 V_T^4 \\ -2(V_{DD} - V_T) R_1 \left( \frac{W}{L} \right)_1 V_T^2 \end{array} \right]$$

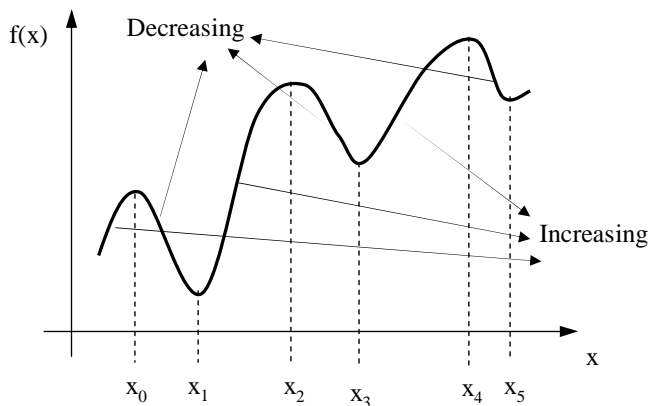
$$a_1 = R_2 K \left( \frac{W}{L} \right)_2 \left[ 4R_1^2 K^2 \left( \frac{W}{L} \right)_1^2 V_T^3 + 2(V_{DD} - V_T) R_1 K \left( \frac{W}{L} \right)_1 V_T \right]$$

$$a_2 = R_2 K \left( \frac{W}{L} \right)_2 \left[ 2(V_{DD} - V_T) R_1 K \left( \frac{W}{L} \right)_1 - 6R_1^2 K^2 \left( \frac{W}{L} \right)_1^2 V_T^2 \right]$$

$$a_3 = 4V_T K^3 \left( \frac{W}{L} \right)_1^2 \left( \frac{W}{L} \right)_2^2 R_1^2 R_2$$

$$a_4 = -K^3 \left( \frac{W}{L} \right)_1^2 \left( \frac{W}{L} \right)_2^2 R_1^2 R_2$$

# Nature of Polynomial Coefficients



**Non-linear, Non-monotonic** function is decomposed into piecewise monotonic functions

# MSDF Calculation

## Definition

**Minimum Size Detectable Fault** ( $\rho$ ) of a circuit parameter is defined as its minimum fractional deviation to force at least one of the polynomial coefficients out of its fault free range

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Maximize  $a_0$

$$\left\{ 1.2 - R_{2,nom}(1+y) \begin{pmatrix} 2.56 \times 10^{-3} + R_{1,nom}^2(1+x)^2 1.024 \times 10^{-7} \\ -5.12 \times 10^{-4} R_{1,nom}(1+x) \end{pmatrix} \right\}$$

subject to  $a_1, a_2, a_3, a_4$  being in their fault free ranges and

$$-\alpha \leq x, y \leq \alpha$$

## MSDF Calculation (contd..)

Assuming single parametric faults,  $\rho$  for  $R_1$

$$\rho = (1 - \alpha)^{1.5} - 1 \approx 1.5\alpha - 0.375\alpha^2$$

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### MSDF for Cascaded Amplifier with $\alpha = 0.05$

Circuit parameter	%upside MSDF	%downside MSDF
Resistor $R_1$	10.3	7.4
Resistor $R_2$	12.3	8.5

# Let us Generalize

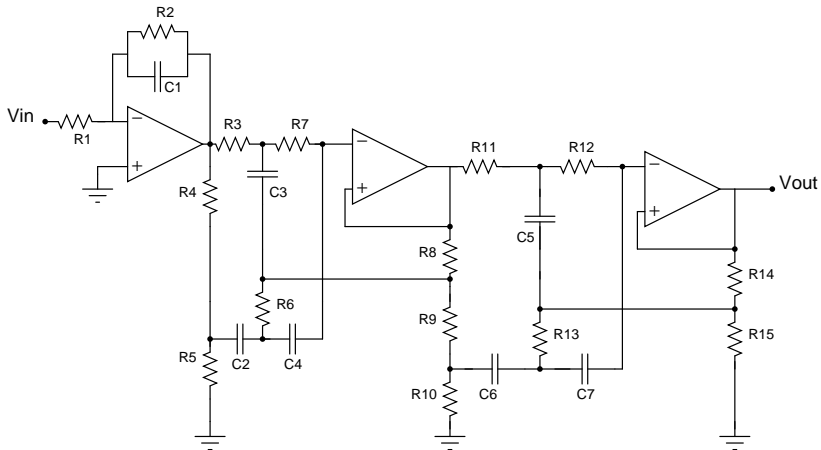
# Generalization – Fault Simulation

- 1 **Start**
- 2 Apply DC sweep to input and note corresponding output voltage levels
- 3 Polynomial Curve fit the obtained I/O data – find the coefficient values of fault free circuit
- 4 Simulate for all parametric faults at the simplex of hypercube
- 5 Find min-max values of each coefficient ( $C_i$ ) from  $i = 1 \dots N$  across all simulations
- 6 **Stop**

# Generalization – Test Procedure

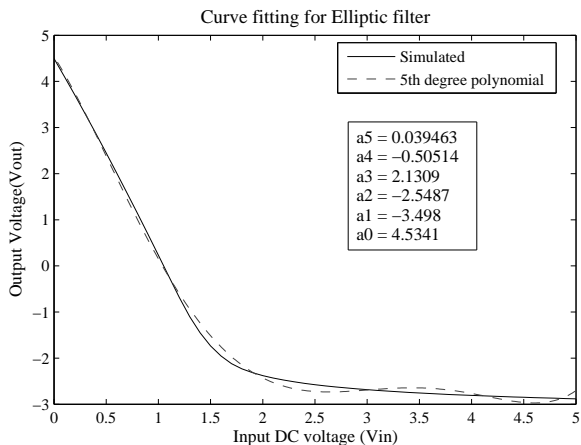
- 1 **Start**
- 2 Apply DC sweep to input and note corresponding output voltage levels
- 3 Polynomial Curve fit the obtained I/O data
- 4 Start with first coefficient
- 5 Consider next coefficient  $C_{i+1}$
- 6  $|C_i| > |C_{i,max}|$  or  $|C_i| < |C_{i,min}|$ ?  
If True go to step 8
- 7  $i < N$ ? If True go to step 4
- 8 Subject CUT to further tests. **Stop**
- 9 **CUT is faulty. Stop**

# Results – Elliptic filter



# Results - Curve fitting

## Curve fit polynomial at 5th order for elliptic filter



$$V_{out} = 4.5341 - 3.498v_{in} - 2.5487v_{in}^2 + 2.1309v_{in}^3 - 0.50514v_{in}^4 + 0.039463v_{in}^5$$

## Results – Elliptic filter

Parameter Combinations Leading to Max Values of Coefficients with  $\alpha = 0.05$

Resistance (ohm)	$a_0$	$a_1$	$a_2$	$a_3$	$a_4$	$a_5$
$R_1 = 19.6k$	18.6k	20.5k	20.5k	20.5k	18.6k	18.6k
$R_2 = 196k$	186k	205k	186k	186k	186k	205k
$R_3 = 147k$	139k	154k	154k	154k	139k	154k
$R_4 = 1k$	950	1010	1010	1010	1010	1010
$R_5 = 71.5$	70	80	80	70	80	70
$R_6 = 37.4k$	37.4k	37.4k	37.4k	37.4k	37.4k	37.4k
$R_7 = 154k$	161k	161k	146k	161k	146k	146k
$R_{11} = 110k$	115k	115k	104k	115k	104k	104k
$R_{12} = 110k$	104k	115k	104k	104k	104k	104k

## Results – Elliptic filter

Parameter Combinations Leading to Min Values of Coefficients  
with  $\alpha = 0.05$

Resistance (ohm)	$a_0$	$a_1$	$a_2$	$a_3$	$a_4$	$a_5$
$R_1 = 19.6k$	20.5k	18.6k	18.6k	20.5k	20.5k	20.5k
$R_2 = 196k$	205k	186k	205k	205k	205k	186k
$R_3 = 147k$	150k	139k	139k	146k	154k	139k
$R_4 = 1k$	1010	950	950	950	950	950
$R_5 = 71.5$	80	70	70	80	70	80
$R_6 = 37.4k$	39.2k	39.2k	39.2k	39.2k	35.5k	39.2k
$R_7 = 154k$	146k	146k	161k	146k	161k	161k
$R_{11} = 110k$	104k	104k	115k	104k	115k	115k
$R_{12} = 110k$	115k	104k	115k	115k	115k	115k

# Results – Elliptic filter

## Results of some Injected Faults

Circuit Parameter	Coefficients out of bounds	Detected
$R_1$ down 25%	$a_0 - a_4$	Yes
$R_2$ down 15%	$a_2, a_5$	Yes
$R_3$ up 10%	$a_1, a_2, a_3$	Yes
$R_4$ down 25%	$a_0 - a_4$	Yes
$R_5$ up 15%	$a_0, a_4$	Yes
$R_7$ up 10%	$a_1, a_2$	Yes
$R_{11}$ up 10%	$a_4, a_5$	Yes
$R_{12}$ down 10%	$a_4, a_5$	Yes

# Fault Diagnosis

## Definition

To determine the circuit parameters responsible for deviation of circuit from its desired behavior.

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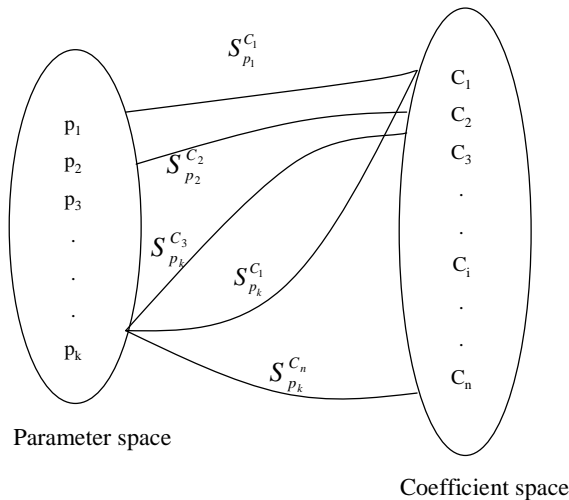
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Sensitivity based diagnosis

$$S_{p_k}^{C_i} = \frac{p_k}{C_i} \frac{\partial C_i}{\partial p_k}$$

# Fault Diagnosis



Possible relation between various parameters and coefficients

# Fault Diagnosis at DC

Fault injected	Coefficient status	Diagnosed fault sites
$R_1$ down 25%	$a_0 - a_4$	$R_1$ or $R_4$
$R_2$ down 15%	$a_2, a_5$	$R_2$
$R_3$ up 10%	$a_1, a_2, a_3$	$R_3$
$R_4$ down 25%	$a_0 - a_4$	$R_1$ or $R_4$
$R_5$ up 15%	$a_0, a_4$	$R_5$
$R_7$ up 10%	$a_1, a_2$	$R_7$
$R_{11}$ up 10%	$a_4, a_5$	$R_{11}$ or $R_{12}$
$R_{12}$ down 10%	$a_4, a_5$	$R_{11}$ or $R_{12}$

# Conclusions and Future Work

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- Technique for parametric fault detection in analog circuits – faults as small as 10% were uncovered
- Diagnosis based on Sensitivity of Polynomial Coefficients to circuit parameters
- **Limitation** – Cannot uncover parametric deviations in reactive elements as input is swept at DC

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- Technique for parametric fault detection in analog circuits – faults as small as 10% were uncovered
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## In future

- Multi-tone polynomial test to uncover parametric faults in reactive elements (*To appear in NATW 2009*)
- Smart Transforms on Polynomial coefficients to capture monotonicity with high sensitivity

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Thanks for your Attention!