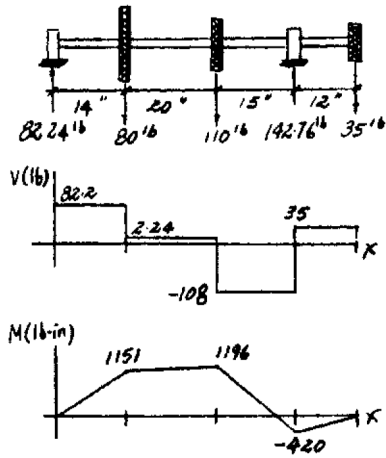
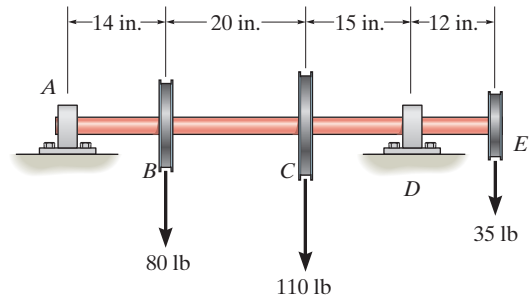
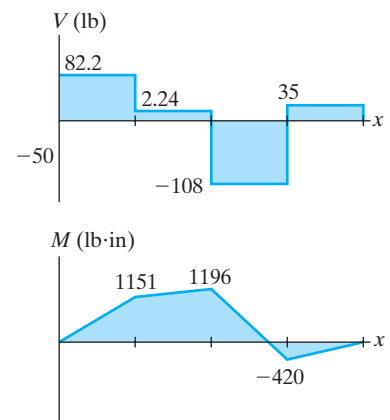


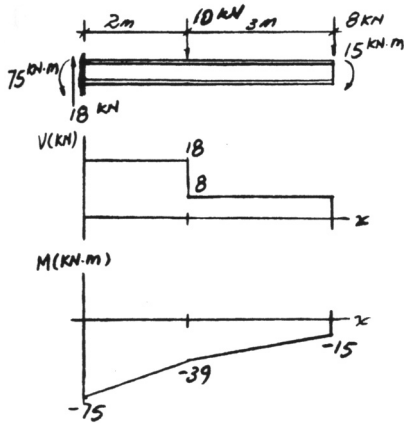
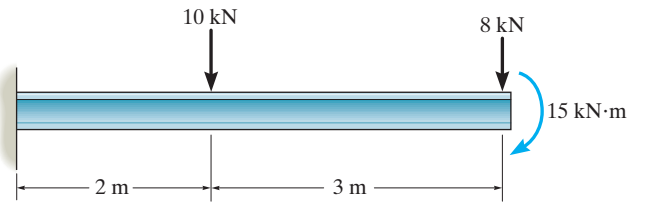
6-2. Draw the shear and moment diagrams for the shaft. The bearings at *A* and *D* exert only vertical reaction on the shaft. The loading is applied to the pulleys at *B* and *C* and *E*.



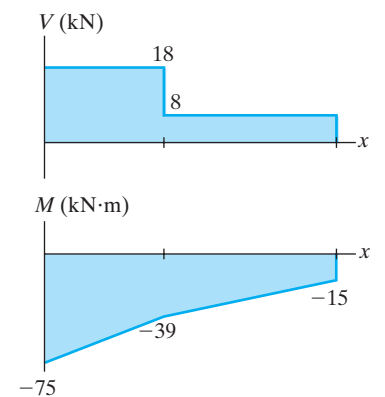
Ans:



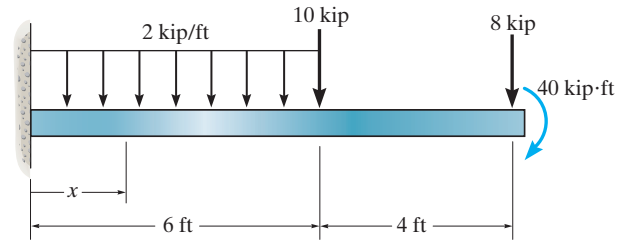
6-5. Draw the shear and moment diagrams for the beam.



Ans:



6-18. Draw the shear and moment diagrams for the beam, and determine the shear and moment throughout the beam as functions of x .



Support Reactions: As shown on FBD.

Shear and Moment Function:

For $0 \leq x < 6$ ft:

$$+\uparrow \Sigma F_y = 0; \quad 30.0 - 2x - V = 0$$

$$V = \{30.0 - 2x\} \text{ kip}$$

$$\zeta + \Sigma M_{NA} = 0; \quad M + 216 + 2x\left(\frac{x}{2}\right) - 30.0x = 0$$

$$M = \{-x^2 + 30.0x - 216\} \text{ kip} \cdot \text{ft}$$

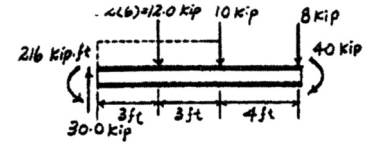
For $6 \text{ ft} < x \leq 10$ ft:

$$+\uparrow \Sigma F_y = 0; \quad V - 8 = 0 \quad V = 8.00 \text{ kip}$$

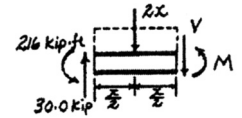
$$\zeta + \Sigma M_{NA} = 0; \quad -M - 8(10 - x) - 40 = 0$$

$$M = \{8.00x - 120\} \text{ kip} \cdot \text{ft}$$

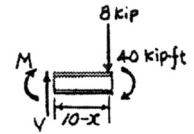
Ans.



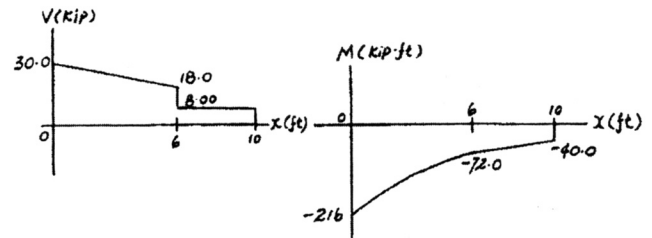
Ans.



Ans.



Ans.



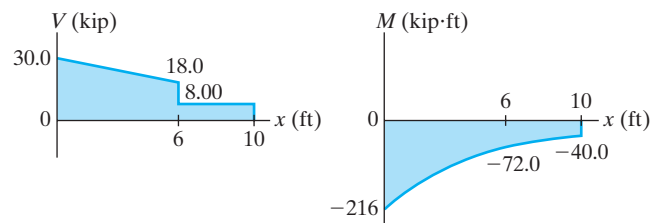
Ans:

For $0 \leq x < 6$ ft: $V = \{30.0 - 2x\}$ kip,

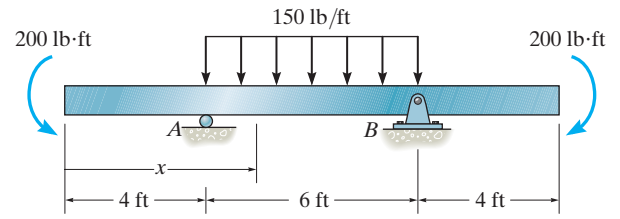
$M = \{-x^2 + 30.0x - 216\}$ kip \cdot ft,

For $6 \text{ ft} < x \leq 10$ ft: $V = 8.00$ kip,

$M = \{8.00x - 120\}$ kip \cdot ft



6-25. Draw the shear and moment diagrams for the beam and determine the shear and moment in the beam as functions of x , where $4\text{ ft} < x < 10\text{ ft}$.



$$+\uparrow \Sigma F_y = 0; \quad -150(x - 4) - V + 450 = 0$$

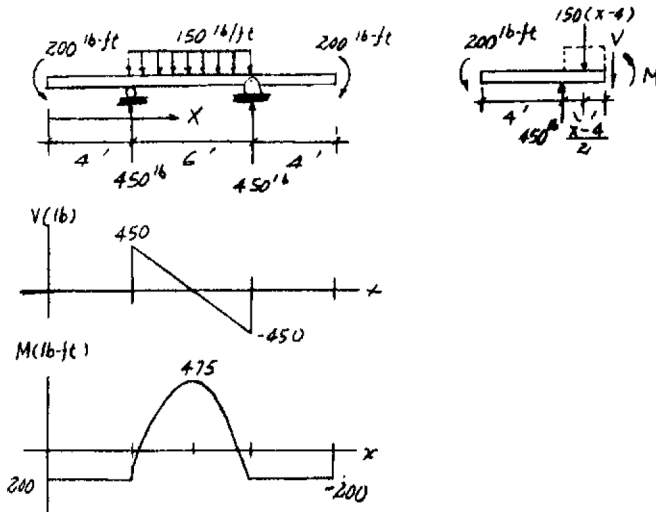
$$V = 1050 - 150x$$

Ans.

$$\zeta + \Sigma M = 0; \quad -200 - 150(x - 4)\frac{(x - 4)}{2} - M + 450(x - 4) = 0$$

$$M = -75x^2 + 1050x - 3200$$

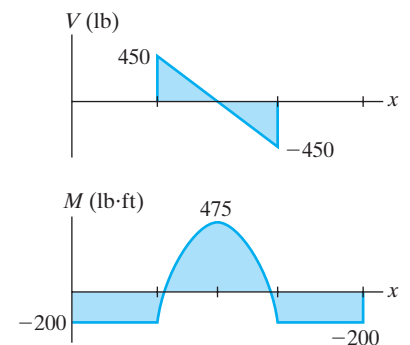
Ans.



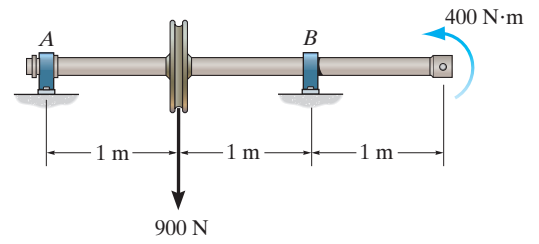
Ans:

$$V = 1050 - 150x$$

$$M = -75x^2 + 1050x - 3200$$



6-33. The shaft is supported by a smooth thrust bearing at *A* and smooth journal bearing at *B*. Draw the shear and moment diagrams for the shaft.



Equations of Equilibrium: Referring to the free-body diagram of the shaft shown in Fig. *a*,

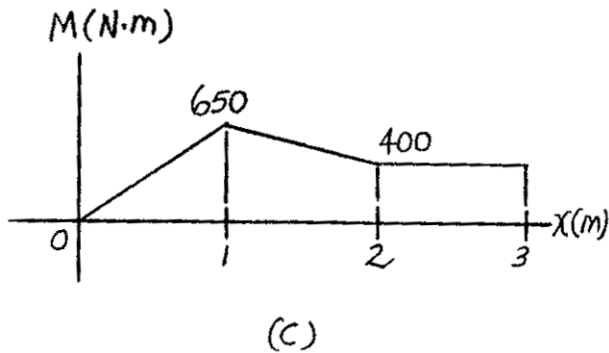
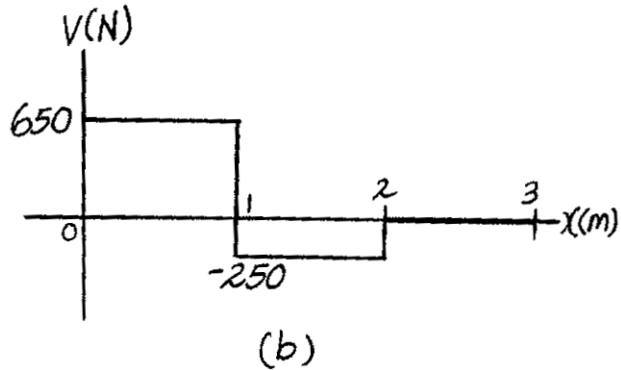
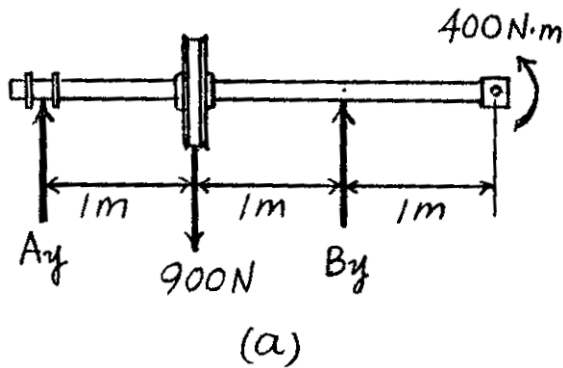
$$\zeta + \sum M_A = 0; \quad B_y(2) + 400 - 900(1) = 0$$

$$B_y = 250 \text{ N}$$

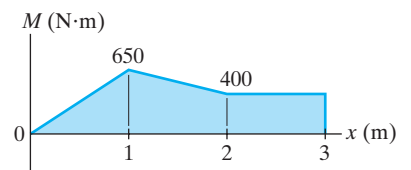
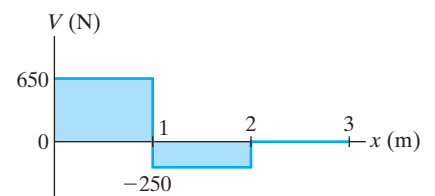
$$+\uparrow \sum F_y = 0; \quad A_y + 250 - 900 = 0$$

$$A_y = 650 \text{ N}$$

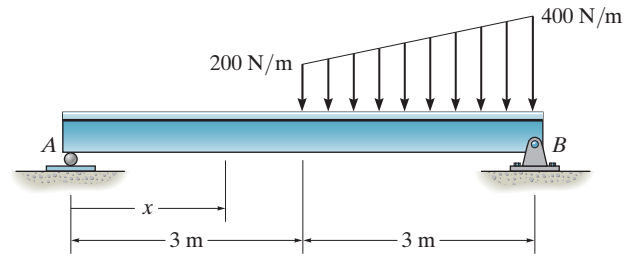
Shear and Moment Diagram: As shown in Figs. *b* and *c*.



Ans:



6-35. Draw the shear and moment diagrams for the beam and determine the shear and moment as functions of x .



Support Reactions: As shown on FBD.

Shear and Moment Functions:

For $0 \leq x < 3$ m:

$$+\uparrow \Sigma F_y = 0; \quad 200 - V = 0 \quad V = 200 \text{ N}$$

$$\zeta + \Sigma M_{NA} = 0; \quad M - 200x = 0$$

$$M = \{200x\} \text{ N} \cdot \text{m}$$

For $3 \text{ m} < x \leq 6$ m:

$$+\uparrow \Sigma F_y = 0; \quad 200 - 200(x-3) - \frac{1}{2} \left[\frac{200}{3}(x-3) \right] (x-3) - V = 0$$

$$V = \left\{ -\frac{100}{3}x^2 + 500 \right\} \text{ N}$$

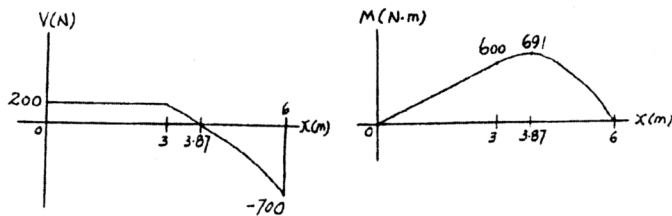
Set $V = 0$, $x = 3.873$ m

$$\zeta + \Sigma M_{NA} = 0; \quad M + \frac{1}{2} \left[\frac{200}{3}(x-3) \right] (x-3) \left(\frac{x-3}{3} \right)$$

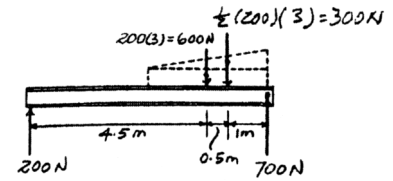
$$+ 200(x-3) \left(\frac{x-3}{2} \right) - 200x = 0$$

$$M = \left\{ -\frac{100}{9}x^3 + 500x - 600 \right\} \text{ N} \cdot \text{m}$$

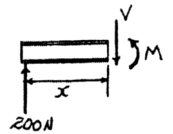
Substitute $x = 3.87$ m, $M = 691 \text{ N} \cdot \text{m}$



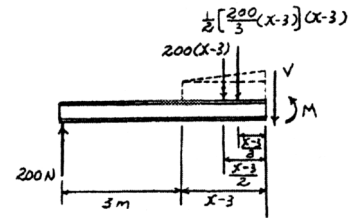
Ans.



Ans.



Ans.



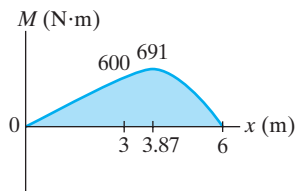
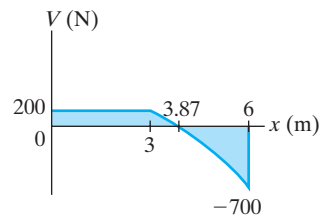
Ans.

Ans:

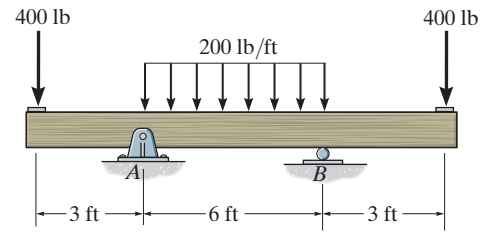
For $0 \leq x < 3$ m: $V = 200 \text{ N}$, $M = (200x) \text{ N} \cdot \text{m}$,

For $3 \text{ m} < x \leq 6$ m: $V = \left\{ -\frac{100}{3}x^2 + 500 \right\} \text{ N}$,

$M = \left\{ -\frac{100}{9}x^3 + 500x - 600 \right\} \text{ N} \cdot \text{m}$



6-39. Draw the shear and moment diagrams for the double overhanging beam.



Equations of Equilibrium: Referring to the free-body diagram of the beam shown in Fig. *a*,

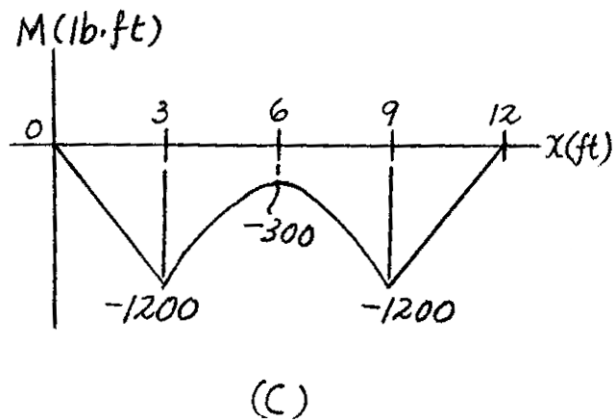
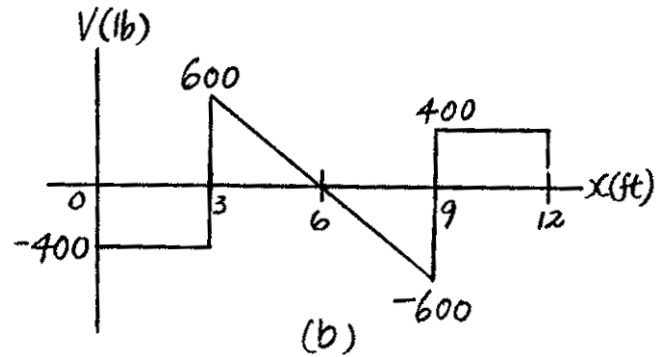
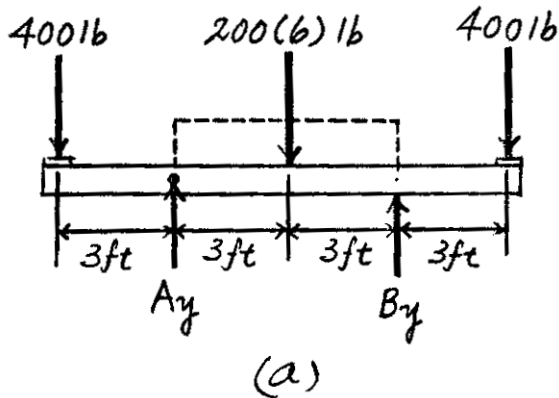
$$\zeta + \sum M_A = 0; \quad B_y(6) + 400(3) - 200(6)(3) - 400(9) = 0$$

$$B_y = 1000 \text{ lb}$$

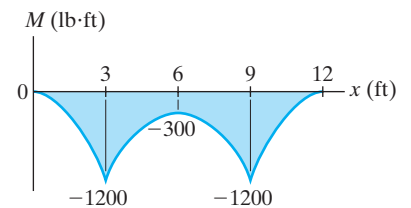
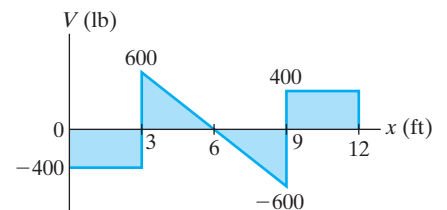
$$+\uparrow \sum F_y = 0; \quad A_y + 1000 - 400 - 200(6) - 400 = 0$$

$$A_y = 1000 \text{ lb}$$

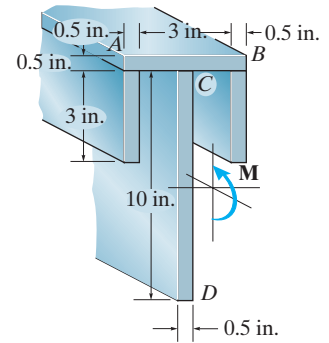
Shear and Moment Diagram: As shown in Figs. *b* and *c*.



Ans:



6-49. Determine the maximum tensile and compressive bending stress in the beam if it is subjected to a moment of $M = 4 \text{ kip} \cdot \text{ft}$.



Section Properties:

$$\bar{y} = \frac{\sum \bar{y}A}{\sum A}$$

$$= \frac{0.25(4)(0.5) + 2[2(3)(0.5)] + 5.5(10)(0.5)}{4(0.5) + 2[(3)(0.5)] + 10(0.5)} = 3.40 \text{ in.}$$

$$I_{NA} = \frac{1}{12}(4)(0.5^3) + 4(0.5)(3.40 - 0.25)^2$$

$$+ 2\left[\frac{1}{12}(0.5)(3^3) + 0.5(3)(3.40 - 2)^2\right]$$

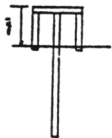
$$+ \frac{1}{12}(0.5)(10^3) + 0.5(10)(5.5 - 3.40)^2$$

$$= 91.73 \text{ in}^4$$

Maximum Bending Stress: Applying the flexure formula $\sigma_{\max} = \frac{Mc}{I}$

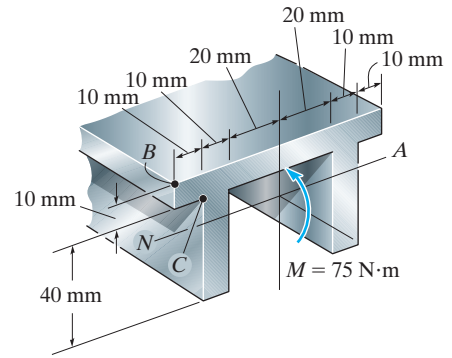
$$(\sigma_t)_{\max} = \frac{4(10^3)(12)(10.5 - 3.40)}{91.73} = 3715.12 \text{ psi} = 3.72 \text{ ksi} \quad \text{Ans.}$$

$$(\sigma_c)_{\max} = \frac{4(10^3)(12)(3.40)}{91.73} = 1779.07 \text{ psi} = 1.78 \text{ ksi} \quad \text{Ans.}$$



Ans:
 $(\sigma_t)_{\max} = 3.72 \text{ ksi}, (\sigma_c)_{\max} = 1.78 \text{ ksi}$

6-59. The aluminum machine part is subjected to a moment of $M = 75 \text{ kN} \cdot \text{m}$. Determine the maximum tensile and compressive bending stresses in the part.



$$\bar{y} = \frac{0.005(0.08)(0.01) + 2[0.03(0.04)(0.01)]}{0.08(0.01) + 2(0.04)(0.01)} = 0.0175 \text{ m}$$

$$I = \frac{1}{12}(0.08)(0.01^3) + 0.08(0.01)(0.0125^2) + 2\left[\frac{1}{12}(0.01)(0.04^3) + 0.01(0.04)(0.0125^2)\right] = 0.3633(10^{-5}) \text{ m}^4$$

$$(\sigma_{\max})_t = \frac{Mc}{I} = \frac{75(0.050 - 0.0175)}{0.3633(10^{-6})} = 6.71 \text{ MPa}$$

Ans.

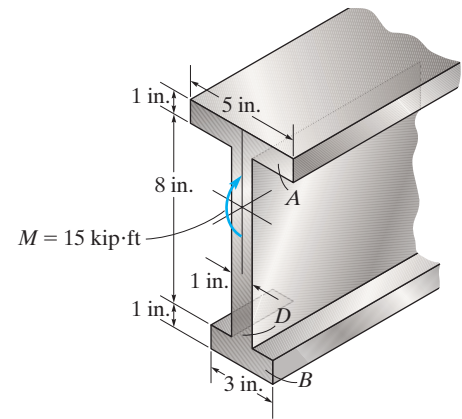
$$(\sigma_{\max})_c = \frac{My}{I} = \frac{75(0.0175)}{0.3633(10^{-6})} = 3.61 \text{ MPa}$$

Ans.

Ans:

$$(\sigma_{\max})_t = 6.71 \text{ MPa}, (\sigma_{\max})_c = 3.61 \text{ MPa}$$

6-61. The beam is subjected to a moment of 15 kip·ft. Determine the percentage of this moment that is resisted by the web *D* of the beam.



$$\bar{y} = \frac{\sum \tilde{y}A}{\sum A} = \frac{0.5(1)(5) + 5(8)(1) + 9.5(3)(1)}{1(5) + 8(1) + 3(1)} = 4.4375 \text{ in.}$$

$$I = \frac{1}{12}(5)(1^3) + 5(1)(4.4375 - 0.5)^2 + \frac{1}{12}(1)(8^3) + 8(1)(5 - 4.4375)^2 + \frac{1}{12}(3)(1^3) + 3(1)(9.5 - 4.4375)^2 = 200.27 \text{ in}^4$$

Using flexure formula $\sigma = \frac{My}{I}$

$$\sigma_A = \frac{15(12)(4.4375 - 1)}{200.27} = 3.0896 \text{ ksi}$$

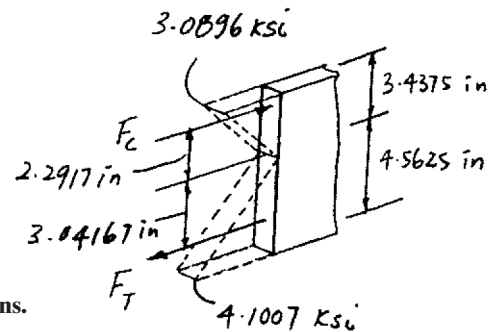
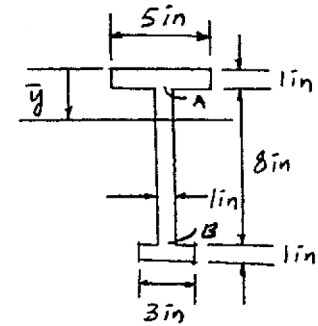
$$\sigma_B = \frac{15(12)(9 - 4.4375)}{200.27} = 4.1007 \text{ ksi}$$

$$F_C = \frac{1}{2}(3.0896)(3.4375)(1) = 5.3102 \text{ kip}$$

$$F_T = \frac{1}{2}(4.1007)(4.5625)(1) = 9.3547 \text{ kip}$$

$$M = 5.3102(2.2917) + 9.3547(3.0417) = 40.623 \text{ kip} \cdot \text{in.} = 3.3852 \text{ kip} \cdot \text{ft}$$

$$\% \text{ of moment carried by web} = \frac{3.3852}{15} \times 100 = 22.6 \%$$

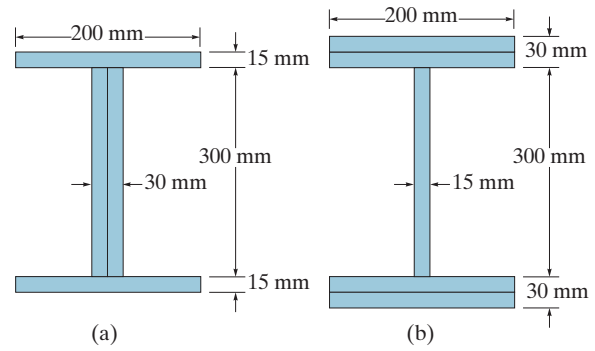


Ans.

Ans:

% of moment carried by web = 22.6 %

6-69. Two designs for a beam are to be considered. Determine which one will support a moment of $M = 150 \text{ kN}\cdot\text{m}$ with the least amount of bending stress. What is that stress?



Section Property:

For section (a)

$$I = \frac{1}{12}(0.2)(0.33^3) - \frac{1}{12}(0.17)(0.3)^3 = 0.21645(10^{-3}) \text{ m}^4$$

For section (b)

$$I = \frac{1}{12}(0.2)(0.36^3) - \frac{1}{12}(0.185)(0.3^3) = 0.36135(10^{-3}) \text{ m}^4$$

Maximum Bending Stress: Applying the flexure formula $\sigma_{\max} = \frac{Mc}{I}$

For section (a)

$$\sigma_{\max} = \frac{150(10^3)(0.165)}{0.21645(10^{-3})} = 114.3 \text{ MPa}$$

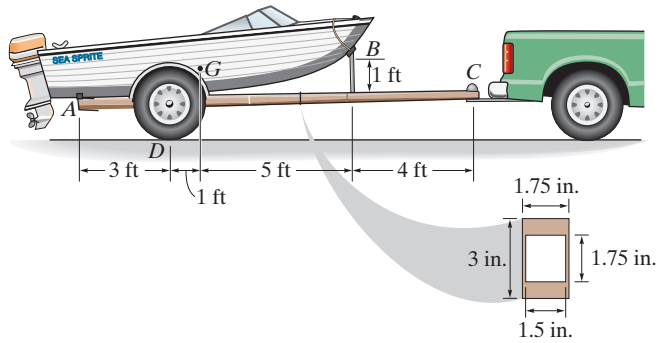
For section (b)

$$\sigma_{\min} = \frac{150(10^3)(0.18)}{0.36135(10^{-3})} = 74.72 \text{ MPa} = 74.7 \text{ MPa}$$

Ans.

Ans:
 $\sigma_{\min} = 74.7 \text{ MPa}$

6-71. The boat has a weight of 2300 lb and a center of gravity at G . If it rests on the trailer at the smooth contact A and can be considered pinned at B , determine the absolute maximum bending stress developed in the main strut of the trailer. Consider the strut to be a box-beam having the dimensions shown and pinned at C .



Boat:

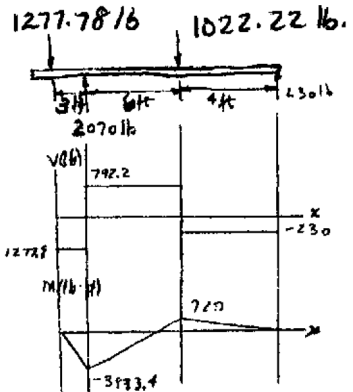
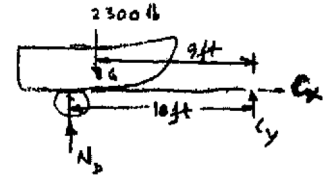
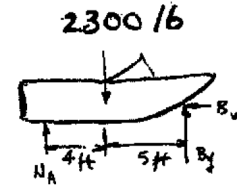
$$\begin{aligned} \rightarrow \Sigma F_x = 0; & \quad B_x = 0 \\ \zeta + \Sigma M_B = 0; & \quad -N_A(9) + 2300(5) = 0 \\ & \quad N_A = 1277.78 \text{ lb} \\ + \uparrow \Sigma F_y = 0; & \quad 1277.78 - 2300 + B_y = 0 \\ & \quad B_y = 1022.22 \text{ lb} \end{aligned}$$

Assembly:

$$\begin{aligned} \zeta + \Sigma M_C = 0; & \quad -N_D(10) + 2300(9) = 0 \\ & \quad N_D = 2070 \text{ lb} \\ + \uparrow \Sigma F_y = 0; & \quad C_y + 2070 - 2300 = 0 \\ & \quad C_y = 230 \text{ lb} \end{aligned}$$

$$I = \frac{1}{12}(1.75)(3)^3 - \frac{1}{12}(1.5)(1.75)^3 = 3.2676 \text{ in}^4$$

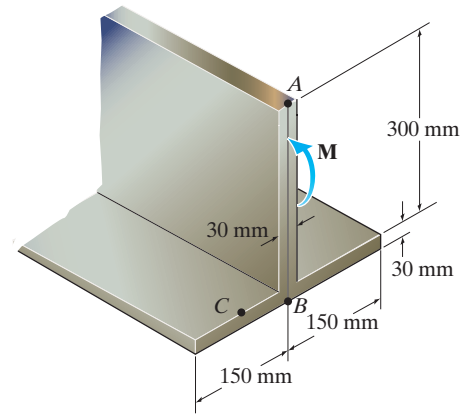
$$\sigma_{\max} = \frac{Mc}{I} = \frac{3833.3(12)(1.5)}{3.2676} = 21.1 \text{ ksi}$$



Ans.

Ans:
 $\sigma_{\max} = 21.1 \text{ ksi}$

6-81. If the beam is made of material having an allowable tensile and compressive stress of $(\sigma_{\text{allow}})_t = 125 \text{ MPa}$ and $(\sigma_{\text{allow}})_c = 150 \text{ MPa}$, respectively, determine the maximum allowable internal moment \mathbf{M} that can be applied to the beam.



Section Properties: The neutral axis passes through centroid C of the cross section as shown in Fig. a . The location of C is

$$\bar{y} = \frac{\sum \tilde{y}A}{\sum A} = \frac{0.015(0.03)(0.3) + 0.18(0.3)(0.03)}{0.03(0.3) + 0.3(0.03)} = 0.0975 \text{ m}$$

Thus, the moment of inertia of the cross section about the neutral axis is

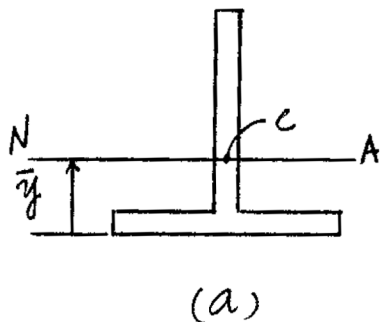
$$\begin{aligned} I &= \frac{1}{12}(0.3)(0.03^3) + 0.3(0.03)(0.0975 - 0.015)^2 + \frac{1}{12}(0.03)(0.3^3) \\ &\quad + 0.03(0.3)(0.18 - 0.0975)^2 \\ &= 0.1907(10^{-3}) \text{ m}^4 \end{aligned}$$

Allowable Bending Stress: The maximum compressive and tensile stress occurs at the top and bottom-most fibers of the cross section. For the top-most fiber,

$$\begin{aligned} (\sigma_{\text{allow}})_c &= \frac{Mc}{I} & 150(10^6) &= \frac{M(0.33 - 0.0975)}{0.1907(10^{-3})} \\ M &= 123024.19 \text{ N} \cdot \text{m} = 123 \text{ kN} \cdot \text{m} \quad \text{Ans.} \end{aligned}$$

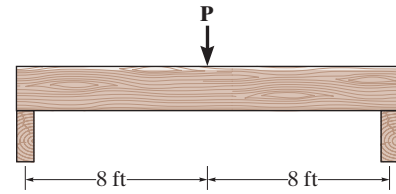
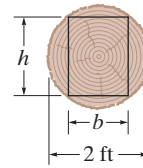
For the bottom-most fiber,

$$\begin{aligned} (\sigma_{\text{allow}})_t &= \frac{My}{I} & 125(10^6) &= \frac{M(0.0975)}{0.1907(10^{-3})} \\ M &= 244\,471.15 \text{ N} \cdot \text{m} = 244 \text{ kN} \cdot \text{m} \end{aligned}$$



Ans:
 $M = 123 \text{ kN} \cdot \text{m}$

6-97. A log that is 2 ft in diameter is to be cut into a rectangular section for use as a simply supported beam. If the allowable bending stress for the wood is $\sigma_{\text{allow}} = 8 \text{ ksi}$, determine the largest load P that can be supported if the width of the beam is $b = 8 \text{ in.}$



$$24^2 = h^2 + 8^2$$

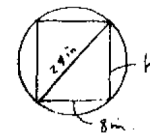
$$h = 22.63 \text{ in.}$$

$$M_{\text{max}} = \frac{P}{2}(96) = 48 P$$

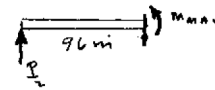
$$\sigma_{\text{allow}} = \frac{M_{\text{max}} c}{I}$$

$$8(10^3) = \frac{48P\left(\frac{22.63}{2}\right)}{\frac{1}{12}(8)(22.63)^3}$$

$$P = 114 \text{ kip}$$



Ans.



Ans:
 $P = 114 \text{ kip}$