

Oscillation for zero input occurs when the system becomes unstable $\rightarrow 1 + AB = 0$
 or $AB = -1$

The condition where $AB = -1 \rightarrow$ called the "Barkhausen criterion"

for $AB = -1 \rightarrow |AB| = 1$ and $\angle AB = -180^\circ$

a. Electronic Oscillators

(1) amplifier provides needed gain so that $|AB| = 1$

(2) passive network provides 180° phase shift

\rightarrow the circuit oscillates at whatever frequency produces 180° phase shift

RL & RC circuits \rightarrow 1 pole per pair \rightarrow up to 90° phase shift

LC circuits \rightarrow 2 poles per pair \rightarrow up to 180° phase shift

\rightarrow |Loop gain| needs to be one at 180° phase shift

or: (1) oscillation may cease: < 1

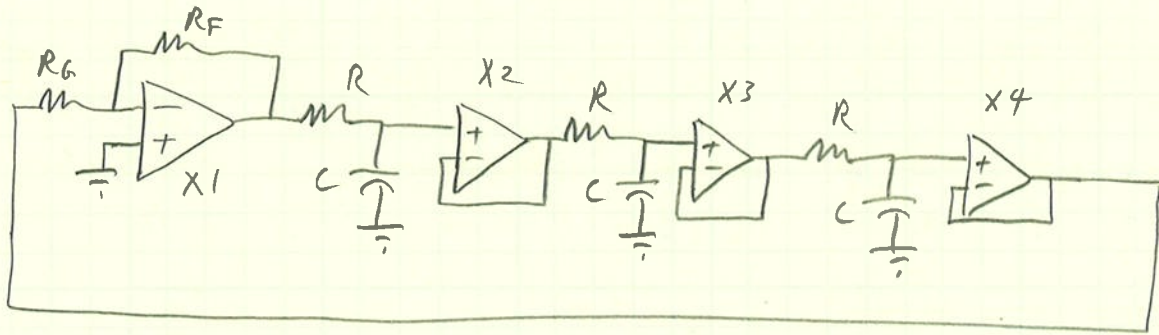
(2) output waveform will be distorted: > 1

\therefore AGC circuit can be used to adjust the gain

to unity at the frequency resulting in a 180°

phase shift, at a desired amplitude.

Ex: Buffered Op amp Phase Shift Oscillator



$R_G, R_F, X_1 \rightarrow$ gain stage \rightarrow gain "A"

\rightarrow each RC stage can produce up to -90° phase shift.

\rightarrow for -180° phase shift \rightarrow each RC stage produces -60° phase shift to generate oscillation

$$AB = A \left(\frac{1}{RCs + 1} \right)^3 \rightarrow -\tan^{-1}(wRC) = -60^\circ$$

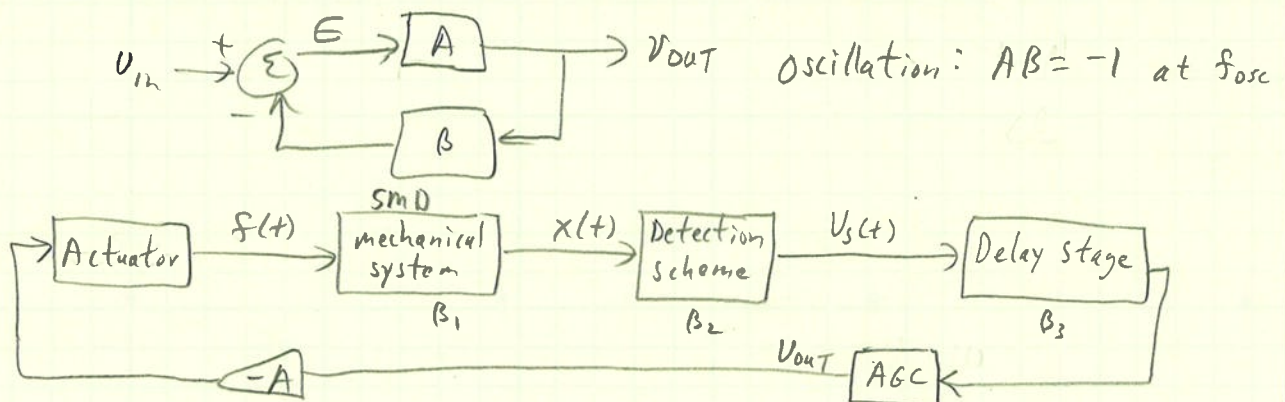
\rightarrow select RC for desired oscillation frequency $\rightarrow f_0$

\rightarrow determine gain A needed for oscillation

\rightarrow size R_G and R_F accordingly

\rightarrow select op amp so that $Af_0 \ll$ GBW product

\rightarrow Now apply this to realize a MEMS electromechanical oscillator \rightarrow a "MEMS Resonator"

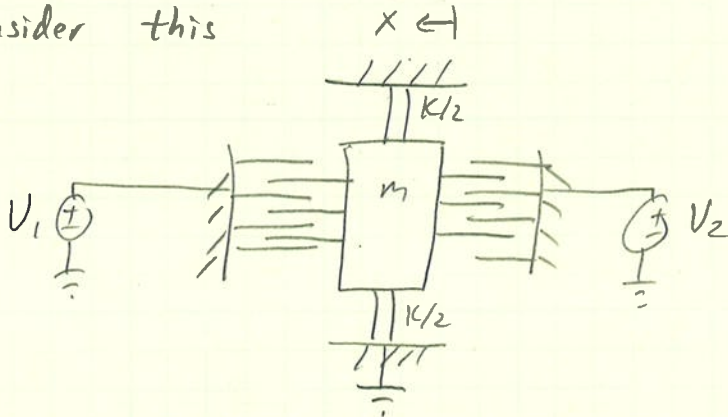


and $f_{osc} : |A B_1 B_2 B_3| = 1$ and $\theta_{B_1} + \theta_{B_2} + \theta_{B_3} = -180^\circ$

For a CDA: $F = \frac{n\epsilon_0\epsilon_r b\beta V^2}{d_0} = \alpha V^2 \rightarrow$ nonlinear function of $V(t)$

If $V(t) = V_1 \cos(\omega t) \rightarrow V^2 = \frac{1}{2} V_1^2 [1 + \cos(2\omega t)] \rightarrow$ not good for making an oscillator

Consider this



let $V_1 = V_B + \Delta V$ and $V_2 = V_B - \Delta V$

$$\begin{aligned} \therefore F_{NET} &= F_1 - F_2 = \alpha V_1^2 - \alpha V_2^2 \\ &= \alpha [(V_B + \Delta V)^2 - (V_B - \Delta V)^2] \\ &= \alpha [V_B^2 + 2V_B \Delta V + \Delta V^2 - V_B^2 + 2V_B \Delta V - \Delta V^2] \\ &= \alpha [4V_B \Delta V] \end{aligned}$$

now Force is linearly proportional to ΔV

Dynamics: $m\ddot{x} + c\dot{x} + kx = f(t)$

$$\text{or } X(s)(ms^2 + cs + k) = F(s)$$

$$\frac{X(s)}{F(s)} = \frac{1/m}{s^2 + \frac{c}{m}s + \omega_n^2}$$

$$\left| \frac{X(j\omega)}{F(j\omega)} \right| = -\tan^{-1} \left[\frac{\omega_n \omega}{\omega_n^2 - \omega} \right] = \Theta_{\text{mech}}$$

$$\Theta_{\text{mech}} \Big|_{\omega = \omega_n} = -\tan^{-1} [\infty] = -90^\circ$$

$$\omega = \omega_n$$

motion lags force by 90° at ω_n