

# Polynomial Coefficient Based Multi-Tone Testing of Analog Circuits

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## Analog Circuit Testing

To determine catastrophic (open or short) faults and fractional deviations in circuit components from their nominal values.

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## In this talk

To propose a method to detect fractional deviations of circuit components from their nominal values in a large class of circuits.

# Outline

- 1 Motivation
- 2 Our Idea
- 3 Generalization
- 4 Results
- 5 Fault Diagnosis
- 6 Conclusion and Future Work

# Motivation

## To Develop an Analog Circuit test scheme

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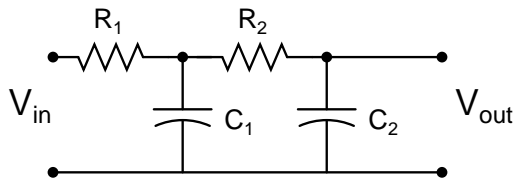
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# Previous Approaches

## Important previous techniques

- $I_{DDQ}$  based test – Intrusive, Area overhead is high  
*[Chakravarty '97]*
- Signal flow graph – Complexity order is high  
*[Bushnell et al. '97]*
- Transfer function based test – Valid only for LTI systems  
*[Savir and Guo '03]*
- Digital assisted analog test – Intrusive  
*[Tim Cheng et al. '06]*
- Polynomial coefficient based test – DC test  
*[Sindia et al. '09]*

# Transfer Function Coefficient Based Test



Second order low pass filter

$$H(s) = \frac{1}{(R_1 R_2 C_1 C_2) s^2 + (R_1 C_1 + (R_1 + R_2) C_2) s + 1}$$

# Our Idea

**Taylor series expansion** of circuit function about  $v_{in} = 0$  at Multi tones

$$V_{out} = f(v_{in})$$

$$V_{out} = f(0) + \frac{f'(0)}{1!} v_{in} + \frac{f''(0)}{2!} v_{in}^2 + \frac{f'''(0)}{3!} v_{in}^3 + \dots + \frac{f^{(n)}(0)}{n!} v_{in}^n + \dots$$

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Ignoring the higher order terms we have

$$V_{out} \approx a_0 + a_1 v_{in} + a_2 v_{in}^2 + \dots + a_n v_{in}^n$$

where every  $a_i \in \mathfrak{R}$  and is bounded between its extreme values for

$$a_{i,\min} < a_i < a_{i,\max} \quad \forall i \quad 0 \leq i \leq n$$

## Our Idea (Contd..)

### In a nutshell

- Find the  $V_{\text{out}}$  v/s  $V_{\text{in}}$  relationship at DC and “relevant” frequencies.

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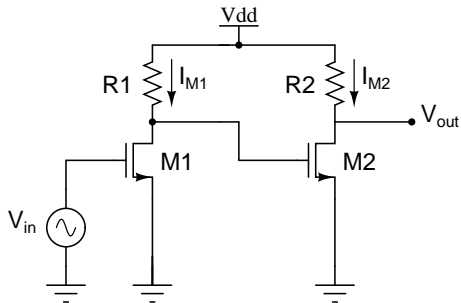
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### In a nutshell

- Find the  $V_{out}$  v/s  $V_{in}$  relationship at DC and “relevant” frequencies.
- Compute the coefficients of fault-free circuit
- Repeat the same for CUT by curve fitting the I/O response
- Compare each of the obtained coefficients with fault-free circuit range
- Classify CUT as **Good** or **Bad**

# Cascaded Amplifiers



Two stage amplifier with 4<sup>th</sup> degree non-linearity in  $V_{in}$

$$v_{out} = a_0 + a_1 v_{in} + a_2 v_{in}^2 + a_3 v_{in}^3 + a_4 v_{in}^4$$

# Polynomial Coefficients

$$a_0 = V_{DD} - R_2 K \left( \frac{W}{L} \right)_2 \left[ \begin{array}{l} (V_{DD} - V_T)^2 + R_1^2 K^2 \left( \frac{W}{L} \right)_1^2 V_T^4 \\ -2(V_{DD} - V_T) R_1 \left( \frac{W}{L} \right)_1 V_T^2 \end{array} \right]$$

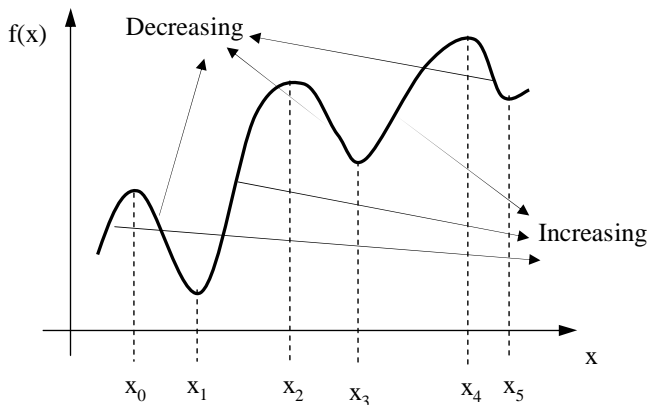
$$a_1 = R_2 K \left( \frac{W}{L} \right)_2 \left[ 4R_1^2 K^2 \left( \frac{W}{L} \right)_1^2 V_T^3 + 2(V_{DD} - V_T) R_1 K \left( \frac{W}{L} \right)_1 V_T \right]$$

$$a_2 = R_2 K \left( \frac{W}{L} \right)_2 \left[ 2(V_{DD} - V_T) R_1 K \left( \frac{W}{L} \right)_1 - 6R_1^2 K^2 \left( \frac{W}{L} \right)_1^2 V_T^2 \right]$$

$$a_3 = 4V_T K^3 \left( \frac{W}{L} \right)_1^2 \left( \frac{W}{L} \right)_2^2 R_1^2 R_2$$

$$a_4 = -K^3 \left( \frac{W}{L} \right)_1^2 \left( \frac{W}{L} \right)_2^2 R_1^2 R_2$$

# Nature of Polynomial Coefficients



Non-linear, Non-monotonic function is decomposed into piecewise monotonic functions

# MSDF Calculation

## Definition

**Minimum Size Detectable Fault**( $\rho$ ) of a circuit parameter is defined as its minimum fractional deviation to force atleast one of the polynomial coefficients out of its fault free range

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Overview of MSDF calculation of R1 with  $V_{DD}=1.2V$ ,  $V_T=400mV$ ,  $\left(\frac{W}{L}\right)_1 = \frac{1}{2} \left(\frac{W}{L}\right)_2 = 20$ , and  $K = 100\mu A/V^2$

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Maximize  $a_0$

$$\left\{ 1.2 - R_{2,nom}(1+y) \begin{pmatrix} 2.56 \times 10^{-3} + R_{1,nom}^2(1+x)^2 1.024 \times 10^{-7} \\ -5.12 \times 10^{-4} R_{1,nom}(1+x) \end{pmatrix} \right\}$$

subject to  $a_1, a_2, a_3, a_4$  being in their fault free ranges and

$$-\alpha \leq x, y \leq \alpha$$

## MSDF Calculation (contd..)

Assuming single parametric faults,  $\rho$  for  $R_1$

$$\rho = (1 - \alpha)^{1.5} - 1 \approx 1.5\alpha - 0.375\alpha^2$$

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### MSDF for Cascaded Amplifier with $\alpha = 0.05$

Circuit parameter	%upside MSDF	%downside MSDF
Resistor $R_1$	10.3	7.4
Resistor $R_2$	12.3	8.5

# Let us Generalize

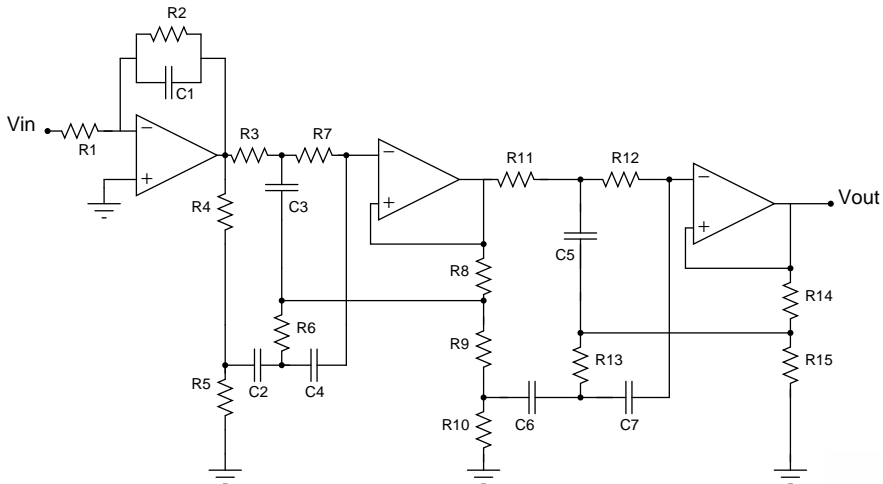
# Generalization – Fault Simulation

- 1 **Start**
- 2 Choose frequency for fault simulation
- 3 Apply sweep to input and note corresponding output voltage levels
- 4 Polynomial Curve fit the obtained I/O data – find the coefficient values of fault free circuit
- 5 Simulate for all parametric faults at the simplex of hypercube
- 6 Find min-max values of each coefficient ( $C_i$ ) from  $i = 1 \dots N$  across all simulations
- 7 Repeat process at all chosen frequencies
- 8 **Stop**

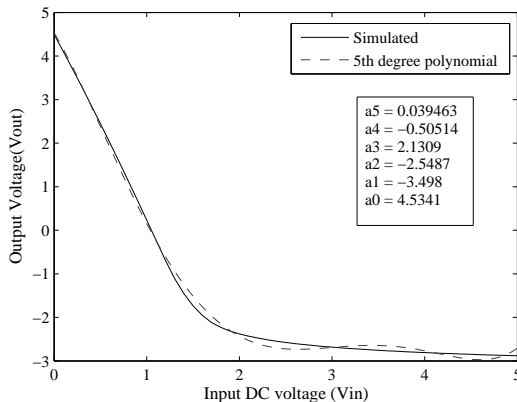
# Generalization – Test Procedure

- 1 **Start**
- 2 Choose a frequency
- 3 Sweep input and note corresponding output voltage levels
- 4 Polynomial Curve fit the obtained I/O data. Obtain coefficients  $C_i \forall i = 1 \dots N$
- 5 Start with first coefficient
- 6 Consider next coefficient  $C_{i+1}$
- 7  $|C_i| > |C_{i,max}|$  or  $|C_i| < |C_{i,min}|$ ?  
If True go to step 11
- 8  $i < N$ ? If True go to step 6
- 9 Repeat steps 2–8 at all desired frequencies
- 10 Subject CUT to further tests. **Stop**
- 11 **CUT is faulty. Stop**

# Results – Elliptic filter

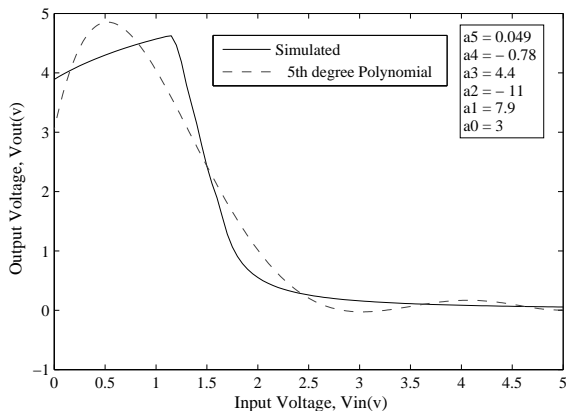


# Results - Curve fitting at DC



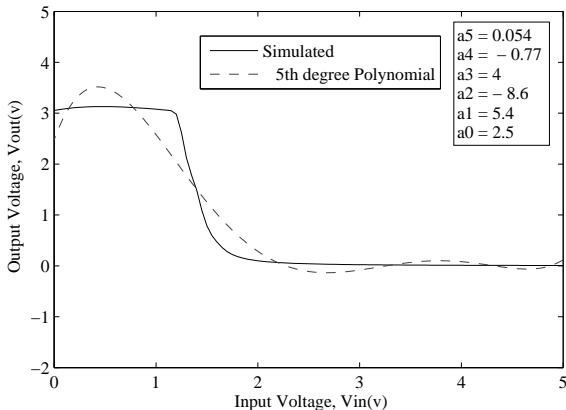
$$V_{out} = 4.5341 - 3.498v_{in} - 2.5487v_{in}^2 + 2.1309v_{in}^3 - 0.50514v_{in}^4 + 0.039463v_{in}^5$$

# Results - Curve fitting at 100Hz



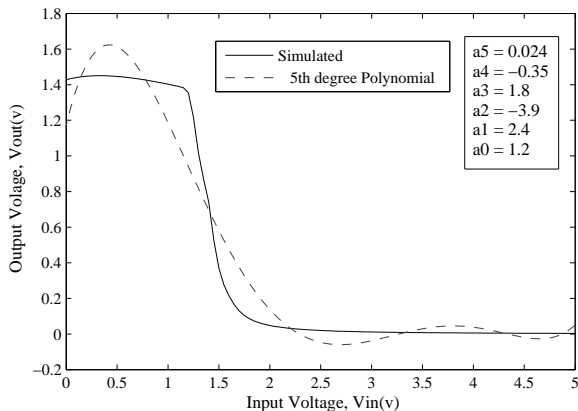
$$V_{out} = 3 - 7.9V_{in} - 11V_{in}^2 + 4.4V_{in}^3 - 0.78V_{in}^4 + 0.049V_{in}^5$$

# Results - Curve fitting at 900Hz



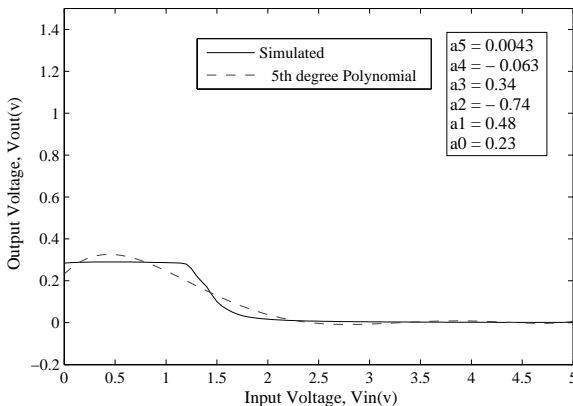
$$V_{out} = 2.5 + 5.4V_{in} - 8.6V_{in}^2 + 4V_{in}^3 - 0.77V_{in}^4 + 0.054V_{in}^5$$

# Results - Curve fitting at 1000Hz



$$V_{out} = 1.2 + 2.4V_{in} - 3.9V_{in}^2 + 1.8V_{in}^3 - 0.35V_{in}^4 + 0.024V_{in}^5$$

# Results - Curve fitting at 1100Hz



$$V_{out} = 0.23 - 0.48v_{in} - 0.74v_{in}^2 + 0.34v_{in}^3 - 0.063v_{in}^4 + 0.0043v_{in}^5$$

## Results at 1000Hz – Elliptic filter

Parameter Combinations Leading to Max Values of Coefficients with  $\alpha = 0.05$  at 1000Hz

Circuit Parameters (Resistance in ohm, Capacitance in farad)						
Nominal Values	$a_0$	$a_1$	$a_2$	$a_3$	$a_4$	$a_5$
$R_1 = 19.6k$	18.6k	18.6k	20.5k	20.5k	20.5k	18.6k
$R_2 = 196k$	205k	205k	205k	205k	186k	186k
$R_3 = 147k$	139k	139k	154k	139k	139k	139k
$R_4 = 1k$	950	950	1.05k	1.05k	1.05k	1.05k
$C_4 = 2.67n$	2.5n	2.8n	2.5n	2.5n	2.5n	2.5n
$C_5 = 2.67n$	2.5n	2.5n	2.5n	2.5n	2.5n	2.8n
$C_6 = 2.67n$	2.5n	2.8n	2.5n	2.8n	2.5n	2.8n
$C_7 = 2.67n$	2.5n	2.8n	2.8n	2.8n	2.8n	2.5n

## Results at 1000Hz – Elliptic filter

Parameter Combinations Leading to Min Values of Coefficients  
with  $\alpha = 0.05$  at 1000Hz

Circuit Parameters (Resistance in ohm, Capacitance in farad)						
Nominal Values	$a_0$	$a_1$	$a_2$	$a_3$	$a_4$	$a_5$
$R_1 = 19.6k$	18.6k	18.6k	18.6k	18.6k	20.5k	20.5k
$R_2 = 196k$	205k	186k	186k	205k	205k	205k
$R_3 = 147k$	139k	139k	154k	139k	139k	139k
$R_4 = 1k$	1.05k	950	1.05k	950	950	1.05k
$C_4 = 2.67n$	2.5n	2.5n	2.8n	2.5n	2.5n	2.8n
$C_5 = 2.67n$	2.8n	2.8n	2.8n	2.8n	2.8n	2.8n
$C_6 = 2.67n$	2.5n	2.5n	2.8n	2.8n	2.8n	2.5n
$C_7 = 2.67n$	2.8n	2.5n	2.5n	2.5n	2.5n	2.8n

## Results at DC – Elliptic filter

Parameter Combinations Leading to Max Values of Coefficients with  $\alpha = 0.05$  at DC

Resistance (ohm)	$a_0$	$a_1$	$a_2$	$a_3$	$a_4$	$a_5$
$R_1 = 19.6\text{k}$	18.6k	20.5k	20.5k	20.5k	18.6k	18.6k
$R_2 = 196\text{k}$	186k	205k	186k	186k	186k	205k
$R_3 = 147\text{k}$	139k	154k	154k	154k	139k	154k
$R_4 = 1\text{k}$	950	1010	1010	1010	1010	1010
$R_5 = 71.5$	70	80	80	70	80	70
$R_6 = 37.4\text{k}$	37.4k	37.4k	37.4k	37.4k	37.4k	37.4k
$R_7 = 154\text{k}$	161k	161k	146k	161k	146k	146k
$R_{11} = 110\text{k}$	115k	115k	104k	115k	104k	104k
$R_{12} = 110\text{k}$	104k	115k	104k	104k	104k	104k

# Fault Detection at Multi-Tones

Injected fault	Coefficients out of Bounds at				Detect
	DC	$f_1=100\text{Hz}$	$f_2=900\text{Hz}$	$f_3=1000\text{Hz}$	
$R_1$ down 15%	$a_0 - a_4$	$a_1 - a_4$	$a_3, a_5$	$a_2, a_4$	Yes
$R_2$ down 5%	$a_2, a_5$	$a_1, a_3$	$a_1, a_5$	$a_1, a_2, a_5$	Yes
$R_3$ up 10%	$a_1, a_2, a_3$	$a_3, a_5$	$a_0, a_3, a_4$	$a_1, a_3, a_4$	Yes
$R_4$ down 20%	$a_0 - a_3$	$a_1 - a_2$	$a_2, a_3$	$a_1, a_2, a_3$	Yes
$C_5$ up 5%	—	$a_0, a_1$	$a_1, a_5$	$a_1, a_2$	Yes
$C_6$ up 15%	—	$a_3, a_4$	$a_1, a_2, a_4$	$a_3, a_4, a_5$	Yes
$C_7$ up 15%	—	$a_1, a_4$	$a_1, a_3, a_4$	$a_1, a_3, a_5$	Yes

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To determine the circuit parameters responsible for deviation of circuit from its desired behavior.

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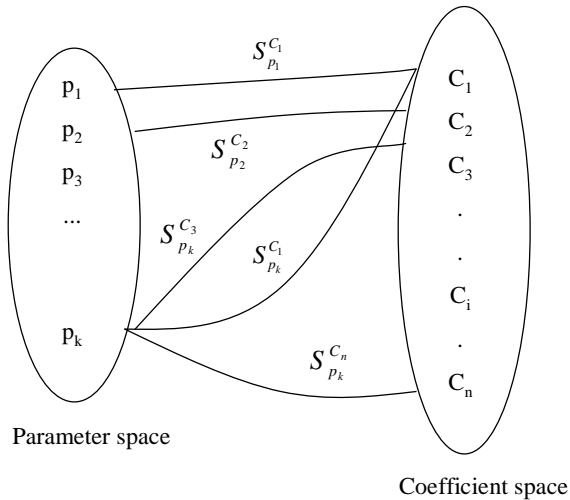
Sensitivity based diagnosis

$$S_{p_k}^{C_i} = \frac{p_k}{C_i} \frac{\partial C_i}{\partial p_k}$$

$$P(\delta p_k | \delta C_i) = \phi \left( \frac{S_{p_k}^{C_i} \delta p_k}{\delta C_i} \right)$$

$\phi$  is any probability measure. We chose negative exponential function

# Fault Diagnosis



# Fault Diagnosis at Multi-Tones

Parametric Fault Diagnosis with Confidence Levels  $\approx 98.9\%$

Injected fault	Diagnosed fault sites at				Deduction
	DC	100Hz	900Hz	1000Hz	
$R_1$ down 15%	$R_1, R_4$	$R_1$	$R_1, R_2$	$R_1, R_2, C_1$	$R_1$
$R_2$ down 5%	$R_2$	$R_2, C_1$	$R_2, R_3, C_1$	$R_2, R_3$	$R_2$
$R_3$ up 10%	$R_1, R_3$	$R_3, C_3$	$R_3, R_4, C_3$	$R_3$	$R_3$
$R_4$ down 20%	$R_1, R_4$	$R_1, R_4$	$R_2, R_4, C_1$	$R_1, R_2, R_4$	$R_4$
$C_5$ up 5%	—	$C_5$	$R_{12}, C_5$	$C_5$	$C_5$
$C_6$ up 15%	—	$R_{10}, C_6$	$C_6, C_7$	$C_6, C_7$	$C_6$
$C_7$ up 15%	—	$C_6, C_7$	$C_7$	$C_6, C_7$	$C_7$

# Conclusions

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- Could uncover parametric deviations in reactive elements as input is swept at DC and selected frequencies
- Technique to diagnose faults through multi-frequency excitation using sensitivity

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- Increasing the sensitivity of coefficients to parameters (to enhance fault coverage), using “smart” transforms
- Techniques for optimal choice of frequencies at which CUT could be excited

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Thanks for your Attention!